Temperature Classification of the Spectra of Dysprosium (Dyi, Dyii)

Arthur S. King,* John G. Conway,** Earl F. Worden,*** and Charlotte E. Moore

Office of Standard Reference Data, National Bureau of Standards, Washington, D.C. 20234

(January 13, 1970)

The Temperature Classifications are listed for 4584 lines of Dy I and Dy II, as taken from an unpublished manuscript of the late A. S. King. In recording his observations, King used a wavelength list compiled mostly from the early literature. A homogeneous and extensive line list based on new observations has been prepared at the Lawrence Radiation Laboratory (LRL). King's data have been edited and adjusted by the present authors to fit the new wavelength list.

In the Table, King's estimated intensities of Dy lines in the spectra of the Arc, Spark, and Furnace are given along with the Temperature Classification. Some of his earlier published work has been used to fill the gaps in this manuscript, which was forwarded to the late W. F. Meggers in 1956.

Key words: Intensity estimates, Dy spectra; dysprosium spectra, temperature classification; temperature classification, Dy I and Dy II; spectra, Dy I and Dy II.

Upon completion of Volume III of "Atomic Energy Levels" in 1958 attention was focused more sharply on rare-earth spectra in preparation for Volume IV, the last of the series. Many of these spectra are complex and have overlapping configurations. The early observations are so fragmentary that it has been necessary to observe the spectra with modern sources and prepare new, homogeneous line lists having spectra of different stages of ionization clearly separated.

In addition, two types of observations are particularly helpful with the interpretation, namely Zeeman Effect and Temperature Classification. The latter subject is uniquely associated with the name of the late A. S. King, who initiated and carried out the extensive program at the Mount Wilson Observatory on estimated line intensities observed in Arc and Spark Spectra and in Furnace Spectra at various temperatures, for many elements. His numerous papers on this subject have helped to lay the foundation of our present knowledge of the structure of complex spectra. An excellent illustration may be found in his work on Gd spectra [1]¹, which enabled H. N. Russell to extend the analyses without the aid of Zeeman data [2].

The present paper is concerned with the first and second spectra of the rare-earth element Dy (Z=66), for which new line lists are available and, also, an extensive list of Temperature Classifications by A. S. King which was unpublished at the time of his death. With the cordial support of R. B. King, the present authors have felt that the material should be published

without further delay. They have assembled the data in Table A, which contains in the first two columns. respectively, the new wavelengths and the spectrum, from the list prepared at the Lawrence Radiation Laboratory (LRL). The following columns are from A. S. King's material; they contain, respectively, his estimated intensities in the Arc, Spark, and High, Medium and Low Temperature Furnace Spectra and the Temperature Classification. The last column contains special notes.

The LRL Line List. The two authors from LRL (J.G.C. and E.F.W.) have selected from their extensive line list the wavelengths and spectral assignments that correspond to the lines observed by King.

The spectra were photographed with the 9.15m Spectrograph at Argonne National Laboratory [3]. The sources were electrodeless lamps containing ¹⁶²DyI₃ prepared and operated as described in references [4] and [5]. The plates were measured on a Grant comparator with photoelectric setting. A thorium comparison spectrum provided the standards. A description of the wavelength reductions may be found in the paper by F. S. Tomkins and M. Fred [6]. The wavelengths are standard air values. They have been rounded off to three decimal places and are listed in column 1 of Table A. The standard deviation ranges from about ± 0.001 Å at 3000 Å to ± 0.01 Å at 9375 Å.

Two methods were used to separate Dy I and Dy II lines: (1) the comparison of relative intensities of lines emitted by electrodeless lamps operated at low and high pressure [5]; (2) the comparison of lines emitted by a spark between Dy metal electrodes and by an electrodeless lamp operated at high Dy vapor pressure. The LRL assignment of the spectrum is entered in column 2 of Table A.

^{*}Present address: Lawrence Radiation Laboratory, Berkeley, Calif. 94720.

^{***}Present address: Lawrence Radiation Laboratory, Livermore, Calif. 94550.

Figures in brackets indicate the literature references at the end of this paper.

The King Line List. This list extends from 3000 Å to 9375 Å. It was forwarded by A. S. King to W. F. Meggers in hand-written manuscript form, in April 1956, evidently with the idea of assisting with the analyses of these complex Dy spectra. Some years later Meggers expressed his desire to one of the present authors (C.E.M.) to have the paper published, but he wished to fill a gap in the observations from $\lambda 3807$ to $\lambda 3903$ before publishing it. He did not live to accomplish this. The present authors have utilized two of King's earlier papers [7] and [8] to help cover this gap and another one from $\lambda 3407$ to $\lambda 3463$.

A few general remarks about the 1956 list are available from correspondence. In a letter to Meggers dated April 4, 1956, King states that "In the first section, λ3000–3800, I did not try to pick out Dy II lines, but I think the criterion will be that Dy I lines maintain their strength in the furnace better than Dy II lines. At higher wavelengths the difference is more pronounced, and I have made the distinction in the

'Class' column."

In a later letter he writes "The λ 's are in general those of Eder throughout the spectrum, in order to have a basic list. Major λ lists are those of J. M. Blank . . . and Harrison, from M.I.T. λ 's. . . . The section 3900–4700 was photographed in the second order and is improved in number of lines by later first-order spectrograms. However, the data from the second-order plates [7] can be used with little change

except for improved wavelengths . . . ".

A considerable amount of editing has been done in fitting the earlier King list to the later much more complete LRL line list. In many cases the disagreement in wavelength is large, amounting in some cases to tenths of an Ångstrom. In fact, within the King line list itself, for a given line several wavelengths are occasionally entered that differ appreciably. These appear to be taken from the earlier literature. Lines for which discrepancies in wavelength exist between the two line lists are indicated by note 3 in the last column of Table A. This note is used for differences exceeding ± 0.05 Å in case King lists the wavelength to two decimals, and for differences exceeding ± 0.1 Å when he lists the wavelength to only one decimal. In spite of large tolerances in $\Delta \lambda$, it is felt that the fitting of the lines from the LRL list to the King list is essentially reliable.

Most of the published papers on Temperature Classification of rare-earths contain only Arc and Furnace intensities. In earlier papers, however, such as one on Ti, King describes in detail the temperature stages and estimated intensities as observed in the High, Medium, and Low Temperature Furnace [9]. In the case of Dy, Arc intensities (column 3, Table A) are given for all lines, and High Temperature Furnace intensities (column 5) for most lines. Intensities from the Medium and Low Temperature Furnace (columns 6 and 7)-exposures are given for only a few of the strongest lines. The Spark intensities in column 4 are all from [7], as indicated by note 1. This reference has been used, also, for two gaps in the 1956 list: λλ3407 to 3463 and λλ3809 to 3831. Users are reminded that in these intervals the intensity scales may not fit smoothly with the rest of Table A.

For lines appearing in both the 1956 list and in reference [7], the arc intensities are the same in many cases; for these the published spark intensity [7] is quoted in Table A, Column 4. In case the 1956 arc intensity differs from that in the 1943 list, the spark intensity published in [7] has been adjusted approximately to the 1956 scale and entered in parentheses in Table A. Examples are as follows:

	λ	Arc	Spark	λ	Arc	Spark
Ref. 7 1956 Table A	3849.388	25 15 15	25 (15)	4111.343	125 150 150	80 (100)

The gap from $\lambda 3836$ to $\lambda 3902$ has been covered in Table A as completely as possible by material from King's 1930 paper [8]. Again, the scale may not fit smoothly on to that of his 1956 ledger, but note 2 in the last column indicates to users that this break exists in the 1956 list. The High Temperature Furnace intensities given in the 1956 list supersede those of 1943 except for the gaps mentioned above.

All lines in the 1943 paper [7] are lines of Dy II according to King. With only one or two exceptions this agrees with the LRL listing. For these lines "E" has been entered in Table A in column 8, which contains the Temperature Classification assigned by A. S. King.

Braces are included in column 8 for lines indicated by King to be double or triple, but unresolved in his list. For example, the pair at $\lambda 6879.015$ to $\lambda 6879.157$ is clearly resolved in Table A, but the intensity estimates

apply to one line in King's list.

A number of lines are blends of Dy I and Dy II. For example, the estimated intensities of the pair at $\lambda 5471.913$ and $\lambda 5471.961$ are entered as blends in Table A. An asterisk in column 5 or 6 indicates that the intensity in the High or Medium Temperature Furnace applies to the Dy I line.

General Comments. A number of King's lines have been omitted from Table A. They fall into three categories: (1) lines for which an Arc intensity is given but no Furnace intensity or Temperature Classification is entered; (2) lines not seen on the new spectrograms used for the LRL list; (3) lines rejected as impurities.

For those lines in King's list where there is a Furnace intensity but no Temperature Classification, a Classification has been added in column 8, on the basis of King's assignments for similar lines and in accordance with the known analysis. Parentheses indicate throughout the entries that have been furnished by the present authors, i.e. entries not taken from the 1956 or earlier lists by King.

The total number of lines in Table A is 4584. Had King lived to edit his list and compare it with the new line list from LRL, the present contribution could have been improved and greatly extended. An earnest effort has been made to interpret and present his data

as reliably as possible.

This work could not have been done without the friendly encouragement of R. B. King, which is greatly appreciated. The authors are, also, most grateful to Isabel D. Murray for her painstaking care in preparing the press copy of the Table.

Table A. Temperature classification of dysprosium lines

	Wave-	Spec-			Intensity			Temp.		Wave-	Spec-		I	ntensity			Temp.	100
	length	trum	1 -	Spark		Furnace		Class	Notes	length (Air)	trum	Arc	Spark	F	Turnace		Class	Note
	(Air)		Arc	Spark	High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low		
3	001.088	I	4					v		3042.238	II	2					V	
	001.649	11	2			-		V		3043.135	ΙI	80	80	2			IVE	1
3	002.384	11	30	25				VE	1	3043.426	ΙI	30	20	1			IVE	1
3	002.862	11	3					V		3043.540	ΙI	10					V	
3	003.756	ΙI	40	20				VE	1	3044.541	II	8					V	
	004.178	H	4					V		3045.231	ΙΙ	1					V	
3	005.045	ΙΙ	1					V		3046.318	ΙΙ	1	} 2				IV	
3	005.935	H	4					V		3046.379		5) 2					
	007.032	ΙΙ	5					V		3046.736	ΙΙ	3					V	
	007.526	ΙΙ	2					V		3047.560	ΙΙ	60	50	2			IVE	1
	008.814	II	10					V		3048.224	ΙΙ	6					V	
	010.034	II	2					V		3048.394	ΙΙ	8					V	
	011.157	II	1					V		3049.119	II	40	30	2			IVE	1
	012.296	II	2					V		3049.638	H	1					V	
	012.629	11	3					V		3050.499	II	3					V	
	013.363	II	2					V		3051.239	II	1		_			V	
	013.452	II	2					V		3051.454	II	60	20	5			IVE	1
	013.698	11	4		_			(V)		3051.818	I			3			IV	3
	014.279	I	1	25	5			IV	,	3052.318	II	40	60				VE	1
	015.068	II	30	25				VE	1	3052.731	II	3					V	
	015.684	II	60	50				VE V	1	3053.198	H	1					V	
	016.598	II	1	60	7				1	3053.686	H	1			4		V	
	016.951	II	40	60				VE V	1	3054.427		1					V	
	017.720 018.272	II	3					V		3054.672	II	4					V	
	018.272 018.956	II	1					V		3055.126	II	1					V	
	016.930 020.340	II	$\frac{1}{3}$					V		3055.858	II	1					V	
	020.340 021.780	H	8					V		3056.964	II	20					V	
	021.780	II	3					V		3057.118	II	4					V	
	022.627	II	3					V		3058.178	II	1					V	
	023.053	11	1					V	3	3058.793	II	3					V	
	024.604	11	1	4				v		3059.473	II	15					V	
	025.412	11	1					v		3060.019	II	20					V	
	025.588	II	25		1			IV		3060.312	II	8	00	,			V	1
	025.746	11	5					V		3060.644	II	80	80	1			VE	1
	026.157	II	150	60	15			IVE	1	3061.365 3061.492	II	30	30				VE VE	$\begin{vmatrix} 1 \\ 1 \end{vmatrix}$
	027.337	11	2	00	10			V		3061.492	II	20 20	15				VE	1
	027.562	II	8					V		3062.163	II	100	80	10			IVE	1
	028.453	11	2					V		3063.248	II	100	00	10			V	1
	028.912	II	1					V		3063.547	II	1					V	
	029.314	11	1					V		3063.880	II	$\frac{1}{2d}$		-			V	
	029.813	11	50	80	-			VE	1	3064.034	II	$\frac{2a}{10}$					V	
3	030.064	H	1					V		3064.565	II	3					v	
3	030.397	11	15					V		3065.174	II	4		-			V	
3	030.786	II	1					V		3065.633	II	2					V	
3	031.194	11	10					V		3066.986	II	60	60	1			VE	1
3	031.532	H	1					V		3067.437	II	3	00	1		-	V	1
3	031.923	ΙΙ	1					V		3068.938	II	6					V	
	032.522	H	1					V		3069.695	II	10					V	
	032.820	ΙI	1					V		3070.458	II	8					V	
	33.194	ΙΙ	20					V		3071.908	II	80	40	15			IVE	1
	033.822	H	1					V		3072.380	II	2	10	10			V	•
	034.484	11	3					V		3072.735	11	4					v	
	035.033	11	1					V		3072.916	II	8					V	
	035.944	11	1					V		3073.539	II	80	80	2			IVE	1
	036.698	11	30	15	2			IVE	1	3073.999	II	2	00				V	1
3	037.387	II	2					V		3074.391	11	1					V	
:	038.285	11	300	300	5			IVE	1	3075.074	11	4					V	
	039.804	11	1					V		3075.178	II	2					V	
	040.262	11	10					V		3075.500	II	6					V	
	041.638	II	12					V		3075.894	II	5					V	
	042.087	1	5					V		JU.J.J.							V	

W/				Intensity			T		W/	C		I	ntensity			T	
Wave- length	Spec- trum		C 1		Furnace		Temp. Class	Notes	Wave- length	Spec- trum		C1	F	urnace		Temp. Class	Notes
(Air)		Arc	Spark	High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low		
3076.888	ΙÌ	20		4			IV		3108.241	II	1					V	3
3078.207 3078.330	I	} 15		5*			IV	3	3109.295 3109.760	II	150	100	10			V IVE	1
3078.682	11	80	60	2			IVE	1	3110.315	II	2	100	10	/		A A F	1
3079.329	ΙI	50	40	1			VE	1	3110.715	I	} 15		2*			IV	<
3080.006	II	2					V		3110.745 3111.544	II)		_			V	
3080.282 3080.918	II	15	-				V		3111.854	II	$\begin{bmatrix} 4 \\ 2 \end{bmatrix}$					V	
3081.911	II	1					V		3112.080	II	3					V	4
3082.510	II	50	15	6			IVE	1	3112.778 3112.870	I	} 5		1*			IV	3
3083.443 3083.557	II	$\frac{2}{2}$					V		3113.104	II							
3084.468	II	3					V		3113.179	I	} 10		3*			IV	3
3084.641	II	15d					V		3113.441	II	1					V	
3084.684 3085.783	II	∫ 3 3					V		3114.297 3115.660	I	1 1			×		V	
3086.627	II	12			-		V		3115.921	II	3					V	
3087.511	II	10		1	a ·		IV		3116.426	I I	1				-	V	
3088.206 3088.412	II	1 5					V		3116.867 3117.423	II	5 2					(V)	3
3088.970	II	1					V		3117.504	II	20					V	
3089.416	H	2					V		3117.960	7,	1					(V)	
3089.597	H	10					V		3117.986 3118.648	II	8 1					V	
3089.775 3090.188	II	4 10					V		3118.963	II	$\begin{vmatrix} 1\\2 \end{vmatrix}$					V	
3090.529	II	2					V		3119.450	II	1					V	
3090.818	I	} 1		4	-	. 0	IV		3120.180	II	80	80	1	-		VE	1
3090.872 3091.930	I	2		2			IV		3120.509 3121.423	II	3 1		, 1			I V	
3092.216	II	1					V	3	3121.987	II	6					V	Į
3093.101	H	60	20	2			IVE	1	3122.115	II	4		15			(V)	
3093.458 3093.730	II	1					V	3	3122.452 3122.943	I	$\begin{vmatrix} 3d \\ 3 \end{vmatrix}$		15			IV V	
3093.730	II	25		1*			IV	3	3123.004	II	1					(V)	
3094.543	II	3					V		3124.896	II	2				-, * *	V	
3095.024 3095.615	II	10 4					V		3126.196 3126.714	II	50	30	2			IVE	1 3
3095.745	II	40	30				VE VE	1	3126.801	II	6		1*	=		IV	
3096.290	II	2					V		3127.259	H	5					V	
3096.898	II	2	,				V	3	3127.475 3128.406	II	4 150	125	5			V IVE	1
3096.995 3097.278	I	3? 1	}	2*			IV	3	3128.757	II	5	125	, ,			\ \A	3 ×
3097.579	II	3					V		3129.302	I	3		20			IV	
3097.655	II	1					(V)	7	3129.764 3130.154	II	1 8					V	
3098.037 3098.523	II	$\begin{vmatrix} 10 \\ 3 \end{vmatrix}$				-	V		3130.561	II	2					V	5
3098.566	II	1					(V)		3131.204	H	2					V	
3099.908	I	1		2			IV	3	3131.467	H	1					V	
3100.915 3101.381	II	$\begin{bmatrix} 6 \\ 2 \end{bmatrix}$					V		3132.121 3132.600	II	6 3		,			V	
3101.361	II	20) 00	20				ſ1	3132.663	. 11	2					(V)	
3101.932	H	50	80	20			IIIE	[1	3133.026	H	6					V	1
3102.197	II	8					V		3133.499 3133.815	II	$\begin{vmatrix} 1\\2 \end{vmatrix}$		25			V	7
3102.786 3103.240	II	$\begin{vmatrix} 1 \\ 60 \end{vmatrix}$	30	1.5			IIIE	1	3134.474	II	$\begin{bmatrix} 2\\2 \end{bmatrix}$		20			V	
3103.828	II	60	60	4			IVE	1	3135.385	11	500	500	30			IVE	1
3104.109	II	10	50	1			IV	1	3135.690 3136.011	II	6 1		20			V III	3
3104.992 3106.046	II	40	50				VE V	1	3136.394	II	$\begin{vmatrix} 1\\2 \end{vmatrix}$		20			V	J
3106.619	II	1			2		V	, ,	3136.692	11	10		1	. :		IV	
3106.970	II	} 5		2*			V	2	3137.558 3138.127	II	1					V	3
3107.041	I)		_				3	3138.127	II	4d					\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	

TABLE A. Temperature classification of dysprosium lines - Continued

Wave-	Spec-			Intensity			Temp.		Wave-	Spec-		I	ntensity			Temp.	
length (Air)	trum	Arc	Spark		Furnace		Class	Notes	length (Air)	trum	Are	Spark		Furnace	T	Class	Notes
				High	Medium	Low							High	Medium	Low		
3138.965	11	2					V		3168.637	ΙΙ	5					V	
3139.497		5					V		3168.954	I	6		. 30			IV V	
3139.887		2					V		3169.558	II	300	100	100			V	1
3140.036 3140.413	1	3 4					V		3170.102	II	40?	100	100			V	1
3140.413	2.	150	150	5			IVE	1	3170.750	11	40	40	1		-	IVE	1
3141.140		200	60	40			IIIE		3170.971	11	20		2			IV	
3141.934		1					V		3171.471	II	20		2		-	IV	3
3142.295	11	40	40	1		1 .	IVE	1	3172.086	II	4					V	£"
3142.624	-	1		5			IV	3	3172.426	I	2	14	1			IV V	
3143.176		15	50	,			V IVE	1	3172.694 3173.017	II	2 2			3 1		V	3
3143.835 3144.224		50	50	, 1			V	3	3173.366	II	1					V	3
3144.500		1					V		3174.017	11	3					v	
3145.218		25		6	14		III		3174.284	ΙΙ	1					V	
3146.160	- 1	60	80	. 2			IVE	1	3174.883	11	30		1			IV	
3146.544	11	1		>			V		3175.538	ΙΙ	1					V	- 3
3146.885		3		1			IV		3176.125	II	2	0				V	
3147.531		30	30	20			VE	1	3176.462	II	4					V	
3147.694		1		20			III V	1	3176.709 3177.213	II	3					V	
3148.164 3149.075		1 3					V		3177.522	II	10					V	
3149.073		3					v		3177.888	II	125	125	2			IVE	1
3149.872		8					V		3178.374	11	60	20	15			IIIE	1
3150.172		25					V		3179.030	ΙI	8					V	
3150.470	11	6				-	V		3180.274	11	3					V	
3150.663		4		5			IV		3180.692	II	5	-			5	V	
3151.310	-	2		,			IV		3181.089 3181.636	II	3 3					V	3
3151.527 3151.890	1	2 50	25	1 5	7		IVE	1	3181.939	II	15		3			IV	"
3152.223		8	20	, ,			V	1	3182.482	II	2	×			5	V	
3152.374		30					V		3183.195	II	8					V	
3153.312		20				4	V		3183.946	11	2					V ·	3
3153.828	3	1		10			IV	3	3184.190	ΙΙ	5					V	
3154.068		5					V		3184.271	II	10					V	3
3154.526		3					V		3184.552 3184.600	II	} 4		1*			IV	3
3154.659 3155.380		5 1					V		3184.787	II	40	25	10			IVE	1
3156.522		500	500	20			IIIE	1	3185.405	I)						3
3157.206		8					V		3185.464	ΙΙ	$\left.\right\}$ 2	n i	1*			ΙV	
3157.55		15					V		3185.967	, II	1					V	
3157.976		3					V		3186.377	ΙΙ	80	60	4			IVE	1
3158.249		2					V		3187.246 3187.680	II	5	60				V	١,
3159.289	1	5 3		3			IV V		3188.372	II	60	60	2	1 1		IVE V	1
3159.304 3159.750		1					V		3188.666	II	5					V	
3159.962		1				*	v		3189.067	II	5			-		v	
3160.503		40	15	5			IVE	1	3189.803	ΙΙ	4					V	
3161.03	11	20	,	2			IV		3190.108	11	1					V	
3161.314		1					V		3190.180	11	3					V	
3162.833		250	250	10			IVE	1	3190.656	II	4					V	
3163.457		10					V		3191.561 3192.035	II	1					V	
3164.041 3164.134		10 15		1			IV	10	3192.035	II	} 5		1*			IV	3
3164.134 r 3164.917		6		, 1			V		3192.139	II	2					V	
3165.264		1					v	3	3192.695	II	2					v	
3165.616		1		5			(IV)		3193.304	II	80	25	25			IIIE	1
3166.304		2					V	3	3193.659	H	3					V	
3166.832		1					V	3	3193.868	H	3					V	
3167.47		25					V		3194.445	II	1					V	
3167.850		15		1	/	1	IV	3	3194.799	II	1					V	
3168.15	11	20		3			IV		3195.886	II	3					V	

TABLE A. Temperature classification of dysprosium lines - Continued

-				Intensity			T ·					I	ntensity				<u> </u>
Wave- length	Spec- trum		, ,		Furnace		Temp. Class	Notes	Wave- length	Spec- trum			F	Turnace		Temp. Class	Notes
(Air)		Arc	Spark	High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low		<
3196.278 3196.429 3197.067	I II II	} 4		2*			IV	3	3223.840 3224.075 3224.595	II	1 3 1					V V	3
3197.595 3198.148 3198.787	I I I I I I	$\begin{bmatrix} 5\\1d\\2 \end{bmatrix}$		4	,	-	IV V		3225.079 3225.153 3225.367	I I I I	25 10 2	} 15	10			{ IVE V	1
3199.233 3199.587 3200.321	II	8 3 } 1		1 8 3*			IV IV	3	3225.947 3226.380 3227.033	II II	80 15 1	60	6			V V	1 ~
3200.632 3200.926 3201.196	II	$\left.\right\}$ 1	,	3*		,	IV	3	3227.419 3227.499 3227.712	II	2 2 5					V V	3
3201.301 3201.660 3202.218	II	15 20 2		2 1 10			IV IV IV		3228.154 3228.598 3228.972	II	1 15					V V	×
3202.597 3202.848 3203.339	11	20 8 1 5					V V V		3229.363 3229.748 3229.939	II	15 1 20		8		*	V V IV	
3203.842 3204.299 3204.357 3204.944	II	6 3 3		2			IV V V		3230.320 3230.663 3230.950 3231.076	II II	6 1 1 1 1					V V V	-4
3205.459 3206.405 3206.642 3207.123	11	30 80 20 60	80 60	1 3	,		V VE V IVE	1	3231.291 3232.092 3232.154	II	1 5 3		0			V V V	
3207.340 3207.774 3208.312	11 11 11	2 1 5	00	3			V	1	3232.645 3233.413 3234.093 3234.416	II II II	30 3 5 2		8	-		V V IV	
3208.813 3208.847 3209.284	11 11	80 8	60	5 1			IVE IV	1 .	3235.085 3235.360 3235.816	II	1 1 120	(100)	7.		, ,	IV V IVE	3 3
3210.066 3210.333 3210.724	II	2 3 1		2			V IV V		3235.894 3236.078 3236.693	11 11	100 4 80	80	6			V IVE	1
3212.045 3212.443 3212.683	II	20 15 20	·	.1			V V		3237.089 3237.857 3238.170	11 11	5 1 4		1			V V	
3213.173 3213.205 3213.587 3213.706	1 I I I I I I I I I I I I I I I I I I I	$\left. egin{array}{c} 4 \\ 1 \\ 2 \end{array} \right.$		3			V V IV		3238.290 3238.693 3238.800	II	6					IV IV IV	3 4
3214.633 3215.193 3215.978	II	25 125 6	125	3 10 1			IV IVE IV	1	3239.190 3239.457 3239.585 3240.037	11 11	1 2 6 8					v V V	3
3216.237 3216.627 3217.151 3217.377	11	3 150 1 15	200	12		-	V IVE V	1	3240.385 3240.721 3240.861	II	2 4 30	30	1			V V IVE	1
3218.012 3218.779 3218.839	11 11	13 1 1 2					V V V		3241.309 3241.717 3242.088 3242.292	1 I 1 I 1 I	$\begin{bmatrix} 3\\1\\2d\\2 \end{bmatrix}$					V V V	
3219.542 3220.128 3220.464	11 11	8 5 25		,			V V V		3242.498 3243.119 3243.723	11 11	$\left.\begin{array}{c} 6\\2\\15d\end{array}\right\}$					V V	4
3221.069 3221.494 3221.637 3221.884	I II II	$ \begin{array}{r} 1 \\ 50 \\ 50d \\ 6 \end{array} $	50 25	4 1 3		٨	IV IVE IVE V	1	3243.784 3244.189 3244.797	I I	2	(100.)	6			V	1
3222.550 3222.875 3223.284	II	1 2 80	80	4			V V IVE	1	3245.124 3245.666 3245.741 3245.877	1 I I I I I I I I I I I I I I I I I I I	$\left. egin{array}{c} 100 \\ 1 \\ 4 \end{array} \right $	(100)	3*			IVE IV V	3

Table A. Temperature classification of dysprosium lines - Continued

W.				Intensity			T		W/	C		I	ntensity			Т	
Wave- length	Spec- trum				Furnace		Temp. Class	Notes	Wave- length	Spec- trum		c 1	F	urnace		Temp. Class	Notes
(Air)		Arc	Spark	High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low		
3246.178	11	2					V		3269.540	II	3					V	
3246.685	11	4					V		3269.947	11	1					V	
3246.802	I	1		5			IV	3	3270.444	II	1					V	
3247.272	II	1					V		3270.939	H	3			,		V	
3248.359	11	50	40	1			IVE	1	3271.307	II	} 2		2*			IV	
3248.893	II	2					V		3271.426	I)		_				3
3249.331	II	2					V V		3271.666 3272.032	II	1 4					V	
3249.414 3249.904	II	2					V		3272.090	II	10					V	
3249.904	II	1					IV		3272.730	II	80	60	1		*	IVE	1
3250.548	II	2					V		3272.961	I	00	00	15			IV	3
3250.987	II)							3273.624	11	1		10			V	
3251.084	I	6		1*			IV	3	3274.208	11	1					V	
3251.268	II	300	300	15			IVE	1	3274.570	11	1					V	3
3251.376	I) 20	1	7.04					3274.609	II	1		,			V	
3251.407	H	$\}. 20$		10*			IV		3274.962	11	2					V	
3251.898	II	50	25	2			IVE	1	3275.743	11	30					V	
3252.189	II	50	- 50	2			IVE	1	3275.928	11	40		2			IV	
3252.638	ΙΙ	1					V		3276.176	ΙΙ	1					V	
3253.223	ΙΙ	1					V		3276.839	II	1					V	3
3253.366	II	1					V		3277.588	II	6					V	
3253.573		1					V		3277.646 3278.330	II	4 6					V	
3253.910	II	12 15		1			IV		3278.396	11	1					V	3
3254.483 3255.148	II	13		1			1 1 4	3	3278.587	II	1				1	V	"
3255.241	II	2		3*			IV		3279.453	II)						
3255.666	I	1		6			IV	3	3279.511	11	30					V	
3256.259	II	80	60	1			IVE	1	3279.696	11	80	60	4			IVE	1
3257.174	I)		- ste					3280.092	11	250	100	30			IIIE	1
3257.226	H	} 15		6*			IV]3	3280:442	11	1					V	
3257.366	II	20					IV)	3280.664	ΙΙ	2.					V	
3258.039	II	2					V		3280.982	11	1					V	
3258.283	II	2					V		3281.650	11	10		1			IV	
3258.890	II	1		0.9			V		3282.059	II	1					V	
3260.021	ΙΙ	3		8?			IV?		3282.504 3282.775	II	3 100	150	1			VE VE	1
3260.701 3260.718	II	} 50	25	10*			IVE	1	3283.083	II	100	150	30			?	3
3261.008	I	2					V		3283.158	II	6		2			IV	"
3261.215	II	30	40				VE	1	3283.556	11	2		_			V	
3261.607	II	1					V		3283.714	11	1		2			IV	
3261.954	II	2	- 4				V		3283.743	ΙΙ	} 4		2			1 1	
3262.042	II	4		1			IV		3284.008	H	3					V	
3262.278	ΙI	6		1			IV		3284.256	ΙΙ	1					V	3
3263.076	II	3					V		3284.365	11	8					V	
3263.186	I	1		10			IV		3284.862	I	3		3			IV	
3263.581	II	1		=			V		3284.878	II	2					V	
3263.908	II	1 1		,			V		3285.443 3285.635	.II	1					V	
3264.300	II	5		1			IV V		3286.151	11	2					V	
3264.744 3265.159	II	4 4					V	-	3286.575	II	10		5			IV	
3265.523	II	10		2			IV		3287.096	I	, 10					1	
3265.998	II)							3287.154	11	$\begin{vmatrix} 2d \end{vmatrix}$		2*			IV	
3266.024	II	60	80	1			IVE	1	3287.170	II			_				
3266.210	II	80	125	1			IVE	1	3287.621	I	1		2*			IV	3
3266.608	II	1					V		3287.807	11	} 1		2*			IV	
3267.259	11	1					V		3287.944	11	50	30	1			VE	1
3267.756	ΙΙ) 0		1			TV		3288.624	I	30		10			IV	
3267.787	II	8		1			IV		3289.103	I	} 6		1*			IV	
3268.075	II	3					V		3289.144	II	J						
3268.278	II	6		2	1.0		V		3289.336	II	5					V	
3268.644	I	2	20	2			IV	1	3289.969	I	1		6			V	1/4
3269.108	II	100	30	15	1.0		IVE	1 1	3290.213	II	1					V	1

Table A. Temperature classification of dysprosium lines - Continued

W /	C.			Intensity			T		W/	S		I	ntensity			Т	
Wave- length	Spec- trum		2 1		Furnace		Temp. Class	Notes	Wave- length	Spec- trum		0 1	F	Turnace		Temp. Class	Notes
(Air)		Arc	Spark	High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low		
3290.647 3291.121	I I	1 15					V		3313.312 3313.854	II	15 1					V	
3292.168	I	1		3			IV		3313.990	ΙΙ	1					V	
3292.615 3293.426	II	3					V		3314.212 3314.583	I	1d		4	-		IV	
3293.420	II	40	15	8			IVE	1	3314.949	II	15		1			V	
3293.876	ΙI	2					V		3315.480	II	3		_			V	
3294.203	ΙΙ	2					V		3315.742	II	4					V	
3294.670 3294.916	II	1					V		3316.316	II	150	60	20		1 -	IVE	1
3294.916	11	$\}$ 6d					V		3316.672 3317.116	II	40	30	6			V IVE	1
3295.202	II	5					V		3317.565	II)	00					1
3295.405	ΙΙ	2					V		3317.601	- II.	$\left.\right\}$ 6d		-			V	
3295.606	II	1			-		V IV		3318.128	I	10		2			IV	-
3295.830 3295.875	I	} 2		$\left\{\begin{array}{c} 6\\4 \end{array}\right.$			V		3318.174 3318.206	II	$ $ $ $					IV	
3296.302	II	40	30	1			VE	1	3318.424	I) .		7.4				
3296.868	ΙI	1					V		3318.483	- II	8		1*			IV	
3297.175	ΙΙ	2	40				V	,	3318.728	ΙΙ	2					V	
3297.603 3298.038	II	30 1	40	4			IVE V	1	3319.038	II	1 8					V	
3298.245	II	,						3	3319.424 3319.682	II	3					V	
3298.362	I	} 10		3*			IV		3319.878	II	400	100	40			IVE	1
3299.149	H	} 4		1*	•		IV		3320.060	I	1		6		-	IV	3
3299.208	I)					V		3320.878	ΙI	1					V	
3299.856 3300.310	II	1 1					V		3321.033 3321.435	II	4					V	
3300.923	II	15					V		3321.878	II	2					V	
3301.490	II	2					V		3322.309	ΙI	1					V	
3301.723	II	3					V	1	3322.925	ΙI	1					V	
3302.016 3302.062	II	2 1					V	}	3323.275 3323.396	I	10		3			IV (IV)	3
3302.401	II	5					v	3	3323.715	II	3		1			V	3
3302.470	ΙΙ	2					V	}	3323.932	II)					v	
3303.170	ΙΙ	} 2					V		3323.962	H	8						
3303.183 3303.667	II	2					V	1	3324.174	II	10					(V)	
3303.715	II	1					v	$\begin{vmatrix} 1 \\ 3 \end{vmatrix}$	3324.215 3324.282	II	3 5					(V)	$ $ $ $ $ $ $ $
3304.012		1					V	ĺį	3324.872	II	2					V	1
3304.069	ΙΙ	1					V	}	3325.277	11	4					V	
3304.294 3304.706	II	6					V		3325.505	II	2		-			V	
3305.400	II	40	30	1	,		IVE	1	3325.590 3325.867	II	4		7			V	
3305.513	ΙΙ	50	40	1			IVE	1	3326.192	II	50	25	8			IVE	1
3306.188	ΙΙ	50	50	1			IVE	1	3326.419	11	8?					V	1
3306.794 3307.427	II	4					V		3326.521	II	6		,			V	3
3308.057	11	3			,		v		3326.987 3327.084	II	$\begin{vmatrix} 1\\20 \end{vmatrix}$	(7)	5			V IVE	$\left.\right\}_{1}^{3}$
3308.287	I	1		6		,	IV		3327.297	II	12	(•)				V	, ,
3308.794	ΙΙ	150	100	3			IVE	1	3327.793	H	2d					V	
3308.884 3309.392	II	300	200	10			IVE V	1	3327.932	II	4		1			IV	
3309.863	11	1					V		3328.796 3329.308	II	15 1		2			IV V	- (
3310.732	11	1					V		3329.798	II	1					V	3
3310.967	11	10					V.		3330.204	II	2					V	
3311.263	11	1					V		3330.599	ΙΙ	10					V	
3311.513	II	5					V		3331.196	II	12		2			V IV	}
3312.328 3312.719	11	100	50	15			IVE	1	3331.275 3332.046	II	12 3		2		,,,	V)
3312.713	I)	55	2*	· 25			3	3332.778	II	3				1	V	
3313.023	II	} 3	×	2*		,	IV		3333.037	H	2					V	
3313.150	II	4					Λ		3333.547	11	5					\ \mathbb{V}	1

Table A. Temperature classification of dysprosium lines - Continued

33 33 33	Wave- length (Air) 333.980 334.137 334.448 334.861 335.460	Spectrum I	Arc	Spark		Furnace		Temp. Class	Notes	Wave	Spec-						Temp.	
33 33 33	333.980 334.137 334.448 334.861		Arc	Spark				Ciuss	Notes	length	trum		6 1	r	urnace		Class	Notes
33 33 33	334.137 334.448 334.861				High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low		
33 33	334.448 334.861	11			4			IV	3	3356.752	II	2d					V	
33	334.861		30	25	1			IVE	1	3357.311	I	1		2			IV	-
		H	15					V		3357.600	II	4 3		1			IV V	
33	335 460	I	6		3			IV V		3357.922 3358.224	ΙΙ	15		2			IV	h
99	335.826	H	$\begin{vmatrix} 2d \\ 8 \end{vmatrix}$					V		3358.300		15		2			IV	}
	335.973	II)							3358.602	11	50	15	10			IVE	1
	336.029	II	$\left.\right \right\} 2d$			- 1		V		3358.952	11	4					V	
	336.515	ΙI	1		1			V		3359.094	ΙΙ	2					V	
33	336.654	I	3		3			IV	3	3359.462	ΙI	40	40	1			IVE	1
7	336.833	ΙΙ	1		1			IV	J	3360.124	I	1 1					V V	
	337.114	ΙΙ	4					V V	3	3360.218 3360.560	II	1					V	
	337.789 338.026	II	$\frac{4}{2}$					V	0	3360.654	II	5					v	
	338.224	II	3					V		3360.936	I	1		5			IV	
	338.613	I	4		1			V		3361.141	11	1					V?	3
	339.066	II	1					V		3361.414	ΙI	4					V	
33	339.509	H	50	30.	8			IVE	1	3361.612	ΙΙ	2					V	
	340.404	II	1		2			V	3	3361.846	II	1 4		3			IV	
	340.614	II	20	200	$\frac{2}{12}$	(4)		IV IVE	1	3362.170 3362.568	II) -					V	
1	340.995 341.429	II	200	200			((IV)	1	3362.600	I	2		3*			IV	
	341.445	I	40	10	10*		{	IVE	1	3362.911	11	1					V	
	341.545	II	2					V		3363.382		8		1			IV	
	341.885	ΙI	80	30	12			IVE	1	3363.481	ΙΙ	3					(V)	
33	342.616	I	} 6		2*			IV		3363.946	ΙΙ	1			,		V	
	342.644	II)							3364.099	I	} 12		10*			IV	3
	343.166	ΙΙ	1					V		3364.337 3364.624	II	2					V	
	343.367 343.510	II	2					V		3365.020	II	$\frac{2}{2}$					V	
	343.524	I	} 4		4*			IV		3365.155	II	1					V	
	343.769	I	2		6			IV	3	3365.806	11	30	30	1			IVE	1
	344.483	I	4		5			IV		3366.235	ΙI	3				-	V	
33	344.826	11	1					V		3366.703	ΙΙ	1					V	
	345.372	11	10					V		3367.207	II	4		١,			I V	
	345.798	ΙΙ	10					V		3367.527 3368.106	II	10 150	50	$\frac{1}{40}$			IVE	1
	346.144	II	12					V		3368.524	II	2	30	40			V)
	346.641 346.662	I	5		1*			IV		3368.640	II	ī					v	3
	347.258	II	2					V		3369.283		10		1			IV	
	347.828	II	40	30	4			IVE	1	3369.638		∫ 8	}	1			IV	
	348.027	II	10					V				2	J				1	
	348.876	II	. 4					V		3369.935 3370.030	I			1*			IV	100
	349.589	II	1		1			IV		3370.030	II	2		1			IV	
	350.298 350.659	II	3 5		1			V		3370.373	II	4		1			IV	
	350.965	II	3					v	1	3370.851	II	40	50	1			IVE	1
	351.286	II	2					V		3370.222	ΙI	1		· ·			V	
	351.736	I	1		5			V		3371.512	11	2		_			V	
	352.217	ΙĮ	6					V	,	3371.692	ΙI	40	40	1			IVE	1 1
	352.688	II	50	60	1			VE V	1 2	3371.806 3372.116	I I	40	40	2 8			IVE	1
	353.234	II	$\begin{array}{c c} 2 \\ 125 \end{array}$	50	25	1		V IVE	3	3372.110	II	$\frac{1}{2}$		0			V	
	353.586 353.913	II	125	30	23			V	1	3372.779	II	8					V	
7	354.211	II	4					V		3373.781	II	2					V	3
	354.686	I	1		5			IV		3374.291	ΙΙ	8					V	
	355.015	II	6					V		3374.958	ΙΙ	1					V	
	355.063	II	10					V		3375.254	II	1					V	
	355.340	II	3					V		3375.739	II	20 15		$\frac{1}{3}$			IV	
	355.593	II	5	40	1			V IVE	1	3375.998 3376.183	II	15		3	- 11		V	7.00
	356.212 356.478	II	$\begin{vmatrix} 40 \\ 2 \end{vmatrix}$	40	1		2, 27	V	1	3376.296	II	10	17.				V	47.14

TABLE A. Temperature classification of dysprosium lines - Continued

				Intensity			T		ayspr		Ī		ntensity				T
Wave- length	Spec- trum				Furnace		Temp. Class	Notes	Wave- length	Spec- trum			F	Turnace		Temp. Class	Notes
(Air)		Arc	Spark	High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low		1
3376.370	11	10					V		3397.726	I	1		2			IV	
3376.548	I	10		6			IV		3397.962	I)		5*				
3376.620	11	15					V		3397.979	II	3					IV	
3376.927	II	1	-				V	3	3398.324		12		2			IV	
3377.101		10		3			IV		3398.789	II	5					V	9
3377.236 3377.744	II	1					\ \		3399.057 3399.175	II	12d		8*			IV	3 ,
3377.788	I	$\left \right 2$		2*			IV		3399.357	II	8					v	
3378.207	II	20		1			IV		3399.586	II	1					V	
3378.416	II	40	30	4			IVE	1	3399.954	I			6		18	IV	3
3378.879	ΙΙ	25	40	8			IVE	1	3400.432	ΙI	3		_			V	
3379.085	II	1					V	3	3400.913	ΙΙ	4		1			IV	1
3379.458 3379.906	I	4		3			IV V		3401.278 3401.687	II	6 2		10	1		V	
3380.164	11	3					v		3401.087	I)			1			
3381.538	II	20		1			IV		3402.009	I	} 10		8*			IV	
3381.917	II	10					V		3402.264	11	1					V	
3382.345	II	1					V		3402.461	ΙΙ	2					V	
3382.718	II	5					V		3402.732	II	6					V	3
3383.409	I	1		8			IV V	3	3402.870	II	4					V	3
3383.670 3384.017	II	1 10		1			(IV)	3	3403.176 3403.244	II	20		4*			IV	3
3384.092	II	8		1			(V)	}	3403.428	II	15					v	
3384.126	II	4					(V)	IJ	3403.810	II	1					V	
3384.797		f 10	}	8			IV	3	3404.600	II	1					V	
	I	3	S		_				3404.944	I	5	}	15*			IV	
3385.015	II	600	400	100	5		IIIE	1	3404.987	II	20	J				IV	
3385.674 3386.348	I	1		5			V IV		3405.314 3405.496	II	$\begin{vmatrix} 1 \\ 6 \end{vmatrix}$		1 1			IV	
3386.568	II	60	80	1			VE	1	3405.653	II	25		6			IV	
3386.967	**	3		1			IV		3406.758	II	8		1			IV	
3387.212	II	15		1			T.17		3406.911	II	2					V	
3387.272	II	} 15		1			IV		3407.159	II	40	30	10			IVE	1
3387.780	II	12		1		-	IV		3407.596	II	1	500	150		4	V	1
3388.076 3388.366	II	10		1			IV V		3407.795 3408.144	II	800	500 60	150			E E	1 1
3388.850	II	100	60	15			IVE	1	3413.785	II	150	80	40			E	1
3389.444	II	20d	00	10			V		3414.821	II	40	30	5			E	1
3389.832	II	1					V		3417.129	ΙI	20	20	1			E	1
3390.084	II	1					V		3418.103	ΙI	20	20	1-			E	1
3390.513	II	2					V		3419.631	II	50	40	5			E	1
3390.786	II	5 30		9			(IV)		3422.864 3425.056	II	25 50	25 20	1 6			E E	1 1
3391.056 3391.162	II	25		3			IV		3429.443	II	60	60	3			E	1
3391.280	II	4		1			V		3431.788	II	30	30	1-			E	1
3391.620	II	1					V		3432.575	- 11	25	15	4			E	1
3391.966	ΙΙ	30		1			IV		3434.368	ΙΙ	250	150	60			E	1
3392.517	I			4			IV		3438.944	H	40	40	1			E	1
3392.772	II	} 4					V		3440.928	II	150	80	2			E E	1
3392.822 3392.973	11	5					V		3441.447 3445.574	II	150 300	60 150	25 80			E	1
3393.363	11	15		3			IV		3446.993	II	60	40	6			E	1
3393.568	II	400	250	80	4		IIIE	1	3449.892	II	30	20	5			E	1
3393.979	ΙΙ	25		1			IV		3454.318	ΙI	200	150	40			Е	1
3394.443	ΙΙ	1					V		3454.510	11	40	40	2			Е	1
3394.841	II	4		1			IV		3456.559	ΙΙ	125	80	10			Е	1
3395.493	II	200	150	50			V	1	3460.968	11	300	150	60			Е	1
3396.157 3396.562	II	200	150	50 3		1	IVE	1	3463.873	II	20	10	3			E	1
3396.800	II	$\begin{bmatrix} 1\\2 \end{bmatrix}$		3)			3468.430	11	60	40	8			IVE	1
3396.863		4		1		}	IV		3468.562	ΙΙ	6			7.		V	
3397.445	I	1		3			IV		3468.784	ΙΙ	10		1			IV.	

Table A. Temperature classification of dysprosium lines - Continued

				Intensity			T					I	ntensity				Ī
Wave- length	Spec-		,		Furnace		Temp. Class	Notes	Wave- length	Spec- trum	0,1	•		Turnace	-	Temp. Class	Notes
(Air)	train	Arc	Spark	High	Medium	Low	Class	litotes	(Air)	l cream	Arc	Spark	High	Medium	Low	Class	litotes
				riigii	.viedidiii ,	LOW		_					Trigii	Wiedium	Low	-	-
3469.132 3469.148	II	$\}$ 2					V		3487.570	II	} 30d	? 40	3			IVE	1
3469.882	II	5					V		3487.605 3487.921	II	1					V	
3470.176	II								3488.192	I	3		8			IV) 3
3470.198	II	} 15		1			IV		3488.308	II	2					(V)	}
3470.577	I	1		3			IV	3	3488.859	H	4					V	
> 3471.077 3471.138	II	60d	40	6			IVE	1	3488.994	II	10		1			IV	
3471.138	II	40	20	3			IVE	1	3489.543 3489.897	II	$\begin{vmatrix} 2\\2 \end{vmatrix}$		10			I V	
3471.606	II	50	30	5			IVE	1	3490.649	II	10				7	V	
3471.803	1	4		8	6		III		3490.880 3490.945	II	3					(V)	
3471.951	II	5		-			V		3490.943	II	$\begin{vmatrix} 2\\4 \end{vmatrix}$					V	
3472.242 3472.595	II	6					V		3492.299	I	2		2		à	IV	
3472.393	I	1)			-				3492.503 3493.086	II	$\begin{vmatrix} 4 \\ 3 \end{vmatrix}$					V	
3472.946	II	} 4		4*			IV		3493.243	I	3		6			IV	
3473.300	II	} 5	,	1*			IV		3493.637	11	1			100		V	
3473.360	I	J							3493.946	H	3					V	
3473.696	II	50	40	6			IVE	1	3494.127	II	15	(15)	1	2		IVE	1
3474.269 3474.296	II	30d	50	8			IVE	1	3494.491 3494.742	II	300	150	100 15			IVE	1
3474.703	II	3		1			IV		3495.322	II	3		13			V	
3475.336	II	3					V		3496.228	11	4					v	
3475.414	II	2	*				V		3496.339	11	50	30	10			IVE	1
3475.657	II	4					V		3496.712	ΙΙ	3		1		- 1	IV	
3476.363	II	8					V		3497.113	I	$ \rangle 2 $		1*			IV	
3476.723 3477.067	II	150	100	50			IVE	1	3497.134 3497.343	11)						
3477.400	H	2	100	30			V	1	3497.378	I	$\left \right $ 1		1*			IV	
3477.528	II	4					V		3497.813	II	40	25	3			IVE	1
3477.927	H	10		1			IV		3498.172	I	1		1			IV	
3478.177	I	3		25	5		III		3498.707	ΙΙ	100	40	5			IVE	1
3478.283	II	6		1			V		3498.934	II	30	15	8			IVE	1
3478.478 3478.761	II	10 3		1			A A		3499.620 3499.862	I	$\begin{vmatrix} 4\\10 \end{vmatrix}$		1			IV	,
3478.877	I	1		6			IV		3499.964	I	8		3			IV	
3479.417	II	2					V	4	3500.512	ΙΙ	5		5			IV	
3479.760	II	6		1			IV		3500.812	11	1					V	
3480.050	II	1		0			IV		3501.288	ΙΙ	1	(4.)				V	
3480.419 3480.811	II	8 20	20	2 3			IV IVE	1	3501.429 3501.859	II	$\begin{vmatrix} 4\\10 \end{vmatrix}$	(4)	1			VE IV	1
3481.144	II	1	20	0,	**		V	1	3502.091	I	4		4			IV	
3481.604	I)		1*			TV		3502.143	11	6					(V)	
3481.623	ΙΙ	} 3		1*			IV		3502.640	I	2		2			IV	
3482.102	ΙΙ	20d	×				V		3502.847	I	3		1			IV	
3482.400 3482.433	II	1 1					V		3503.025 3503.174	II	2			- 4		V	
3482.772	II	10	2 1				V		3503.174	II	$\left.\right\}$ 20d		3			IV	
3483.073	II	1					V		3503.365	II	3					V	
3483.315	I	3		8			IV		3503.663	H	2	1		128.		V	
3483.556	ΙΙ	1	,				V		3503.784	11	1	J					3
3484.190	I	$\frac{3d}{6}$		15	2		V		3504.116	H	1					V	3
3484.522 3484.676	II	8 40	30	3	0		IVE	1	3504.498 3504.529	II	80 d	80	8	5		IVE	1
3484.881	II	5	30	, ,			V	1	3504.936	II	4			- 7		V	
3485.408	II	1			3		V		3505.171	II	3			1941		V	
3485.436	ΙΙ	3			1 1/2		V		3505.420	H	} 50	40	{ 8	}		?E	1
3485.660	II	1					V	1.6	3505.453	II	J		5	J		1.0	1
3485.918 3486.146	II	20 3		1			IV		3505.561 3505.844	II	$\begin{vmatrix} 3\\20 \end{vmatrix}$	10	5			V IVE	1
3486.945	II	3					V		3506.038	II	20	10	3		Ty.	V	1
3487.197		15		3			IV	32 H	3506.247	II	3		1	1.7.		IV	122
		Variable .															

				Intensity								I	ntensity				
Wave- length	Spec- trum				Furnace		Temp. Class	Notes	Wave- length	Spec- trum			F	urnace		Temp. Class	Notes
(Air)		Arc	Spark	High	Medium	Low			(Air)	c	Arc	Spark	High	Medium	Low		
3506.638 3506.813	II	1 150	50	30	cuidin	20.1	V	1	3526.839 3526.905	II	4 8				Eo II	(V)	
3507.534 3507.694	I	2	,	2*			IV		3527.088 3527.178	I	8		10	3*		III	3
3508.031	I)		1*			IV	3	3527.707	I	1		15	1		IV	3, 4
3508.095 3509.012	II	3		•			V		3527.993 3528.472	II	$\begin{array}{c c} 6 \\ 2 \end{array}$		1			IV V	
3509.012	II	20		3			IV	3	3528.861	I	,						<
3509.434	II	4					V		3528.896	II	} 3		1*	,		IV	
3510.053	ΙI	3					V		3529.030	11	6		1			V	
3510.155 3510.872	II	3 2	>				V		3529.148 3529.563	II	15 1		2			V IV	
3511.014	I	5		25	15	5	II		3530.047	11	1				- "	V V	2
3511.368	ΙΙ	2					V		3530.371	I	2		20	4		III	
3511.685	II	20	-	1 1			IV		3530.566	II	8					V	1
3511.974 3512.078	11	4		1			V		3530.954 3531.706	II	2000	1500	500	100	5	V IIIE	1
3512.556	II	20	20	1			IVE	1	3532.427	I	4	1000	1	100		IV	
3512.699	II	30	40	1			VE	1	3532.536	I	3		1			IV	
3513.046 3513.208	II	$\frac{2}{2}$					V		3532.884 3533.262	I	1		3 3			IV	
3513.516	I	_		5			IV		3533.638	I)						
3513.734	II	2					V		3533.749	ΙΙ	3		5*			IV	<
3513.891 3514.131	I	3 5		4			IV V		3534.033	I	4		15	4		III	
3514.131	II	,		7.16					3534.450 3534.508	I	20		4*			IV	
3514.591	I			1*		V.	IV	3	3534.959	II	200	100	80	8		IIIE	1
3514.732	I	} 1		1*			IV	3	3535.186	11	2	-				V	
3514.795 3515.097	II	$\frac{1}{2}$		3		V	IV		3535.630 3536.019	II	$\frac{2}{400}$	400	80	3		V IVE	1
3515.614	II	4					(V)	1	3536.512	II	15	400	00	3		(V)	1
3515.769	I	1		25	3		III	5	3536.585	I	2		3			(IV)	
3516.112 3516.511	II	1 1					V		3536.860	II	2					V	
3517.050	11	1				4	V	3	3537.174 3537.665	II	1 6					IV)
3517.261	II	60	50	8			IVE	1	3537.763	I	2		3			IV	}
3517.625	I	2		8			IV V		3538.056	ΙΙ	1					V	
3517.934 3518.721	II	1 1					IV		3538.517 3538.852	II	300	150	100	6		IIIE V	1
3519.104	II	1					V		3539.368	II	1						,
3519.665	II	6					(V)		3539.386	I	30	20	15*	,		IVE	1
3519.765 3519.903	II	6 8					(V)		3539.643	ΙΙ	10		1			IV	× ×
3520.349	II	1					V		3539.896 3540.232	I	$\begin{vmatrix} 4\\2 \end{vmatrix}$		4 5			IV	3
3521.157	I	§ 15	}	25	6		III		3540.687	II	8		1			IV	
3521.491	I	20	J	3			IV	3	3541.301	ΙΙ	3		1			IV	<
3521.491	II)			. ,			3	3541.579 3541.824	II	1 4		1			IV	
3521.897	ΙΙ	6		1			IV		3542.327	II	150	100	30			IVE	1
3522.277	II	$\frac{10d}{2}$		2			IV V	-	3542.420	I	7		4	-		IV	3
3522.672 3522.861	II	2 15		3			IV		3542.865	II	5		1			IV	
3523.208	II	2?	}	15	1*		IV		3543.132 3543.826	II	2 3	*	1 1			V	
3523.254	I	2	J						3544.038	II	4					V	1
3523.455 3523.982	I	1 400	300	10 100	2 2		IVE	1	3544.204	11	25	20	4			IVE	1
3524.574	II	2	500	100			IV	1	3544.347 3544.992	11	20 30	20	3 4			IVE	-1-
3524.633	I	6		3			IV		3545.259	II	1		4			V	1
3524.930	II	8?d		3			V	.,	3545.625	11	2		,			V	
3525.746 3526.566	II	15 2		3	1		IV (V)	1	3545.768	II	5					V	
3526.637	II						V		3546.002 3546.105	II	1					V	}
						•	1				•						1 '

 $Table \ A. \ \textit{Temperature classification of dysprosium lines} - Continued$

W/				Intensity			T		Wave-	C		I	ntensity			T	
Wave- length	Spec- trum		C 1	×	Furnace		Temp. Class	Notes	length	Spec- trum		6 1	F	Turnace		Temp. Class	Notes
(Air)		Arc	Spark	High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low		
3546.831	11	100	50	50	2		IVE	1	3571.438		ſ 1	1	30	10	4	III	
3547.008	II	3					V			I	3	5	30	10	*	111	
3547.538 3547.912		10		1			IV (V))	3571.667 3571.740	II	} 6		10	1*		IV	
3547.912	I	$\frac{1}{6}$		6	3		III	$\left \right _{3}$	3572.094	II	1			-	, -	V	
3548.192	II	15	(15)	2			IVE	1	3572.389	I	1		5			IV	
3548.717	II	8		1			IV		3572.654	11	2			3.0		V	
3549.248		300	200	2 80	2		IVE	1	3573.026 3573.063	I	} 6		1*			IV	
3550.218 3550.986	II	2	200	00			V	1	3573.318	II	1		8	2		III	3
3551.148	I	5		6			IV		3573.830	II	60	50	4	_		IVE	1
3551.616	II	150	100	30			IVE	1	3574.006	I			2			IV	
3552.021	II	2	3				IV		3574.153	ΙΙ	100	60	15		-	IVE	-1
3552.289 3553.160	II	$\begin{vmatrix} 1\\2 \end{vmatrix}$					V		3574.620 3574.903	II	1 1					V	
3553.100	11	$\frac{2}{2}$	4	4			IV		3575.379	II	2					v	
3554.855	H	2			,		V		3575.600	I	2		3			IV	
3555.328	I	2		3			IV		3576.004	I	10		3			IV	
3555.677	II	3		,			V		3576.244	ΙΙ	300	200	50	1		IVE	1
3555.970 3556.420	II	10		1			IV V		3576.580 3576.866	II	5 150	100	25	1		V IVE	1
3556.550	I	1		1			IV	3	3577.460	II	130	100	2.5	1		V	
3556.842	I	} 2		8*			IV	3	3577.649	II	4					V	
3557.010	II)			7			3	3577.982	ΙΙ	60	30	25			IVE	-1
3557.181	I	2		10			IV		3578.501	I	3		2			IV	
3557.622 3558.117	II	$\frac{10}{2}$		1	-		IV V		3578.832 3579.113	I	3 5		3 5			IV	
3558.232	II	8		5			IV		3579.437	I	$\frac{3}{2}$		1			IV	
3558.511	I	3		3			IV		3580.035	II	40	30	8			IVE	1
3559.295	II	15		2			IV		3581.847	ΙΙ	1	(70)				V	١,
3559.564 3560.139	11	1		1			IV		3582.021 3583.459	II	10	(10)	$\frac{2}{10}$	2		IVE	$\begin{vmatrix} 1 \\ 3 \end{vmatrix}$
3560.207	I	} 10		4*			IV		3584.417	I	40	40	3			IVE	1
3560.409	II	1		5			IV		3585.058	II	250	100	50	3		IVE	1
3561.263	H	2		_			V	3	3585.778	ΙΙ	150	80	20			IVE	1
3562.696		5 200	100	2 40	1		IVE	1	3586.112	II	50	30	10	5		IVE	$\frac{1}{3}$
3563.148 3563.395	I	200	100	3	1,		IV	1	3589.457 3590.074	I	30	25	2	5		(III)	1
3563.692	II	40	50	3			IVE	1	3590.658	II	25	20	2	1		IVE	î
3564.237	I	8		15			IV		3591.415	ΙΙ	125	80	20			IVE	1
3564.561	II	2					V		3591.811	ΙΙ	40	40	5			IVE	1
3564.768 3565.116	II	1 1					V		3591.982 3592.107	I	$\frac{1}{30}$	30	10 10	- ^		IV IVE	1
3565.269	II	1				14	v	3	3592.107	II	2	30	10	× ,		V	3
3565.686		5		1			IV		3593.047	II	1		1			IV	3
3566.055	II	4					V		3593.160	I	4		1			IV	
3566.099 3566.561	II	$\frac{1}{2}$					V		3593.676	II	} 2		20	1*		IV	9
3566.785	I	2		3			IV		3593.773 3594.283	I	2					V	
3566.886	II	2					V		3594.480	I	4		5			?	
3567.299	I	3		1			IV	7 -	3594.560	I	5	105	30	8		III	,
3567.620	I	1		4			IV		3595.036 3595.283	II	125	125	20 1	8.7		IVE V	1
3568.035 3568.363	II	3 5				8	V		3595.648	II	1		1			IV	1.4
3568.408	II	3					V		3596.058 3596.481	II	40	30	6			IVE	1
3568.727	I	1		8			TV		3596.987	II	1		1	*		V	3
3568.739	I	$\left.\right\}$ 1		ð			IV		3597.284	I	3		25	3		III	
3569.010	II	4		6			V	9	3597.537	I	1			1		(III?)
3569.332 3569.660	I	$\begin{array}{c c} 2\\20 \end{array}$	10	6 8			IVE	$\begin{vmatrix} 3 \\ 1 \end{vmatrix}$	3597.742 3597.936	II	1 8		1			(V)	
3571.023	II)	10						3598.256	II)						
3571.063	I	3	110	1*			IV		3598.319	I	} 10		6*	,		IV	

TABLE A. Temperature classification of dysprosium lines - Continued

W	Small			Intensity			Torre		Wave-	Spec-		I	ntensity			Temp.	
Wave- length	Spec- trum		C 1	Y Y	Furnace		Temp: Class	Notes	length	trum		C 1	F	Turnace		Class	Notes
(Air)		Arc	Spark	High	Medium	Low			(Air)	*	Arc	Spark	High	Medium	Low		
3598.726 3599.038 3599.471 3600.253 3600.297	I II II II	$ \begin{array}{c} 1\\3\\4\\ \end{array} $	40	2 1 1 10			IV IV IV	},	3622.350 3622.560 3622.588 3622.769 3623.127	I II II I	4 1		2* 8	9		IV V IV	3
3600.376 3600.632 3600.946	11	$ \begin{array}{c c} 50d? \\ 1 \\ 1 \\ 5 & 2 \end{array} $	40	30			V V	3	3623.385 3624.267 3624.900 3625.528	III	$\begin{bmatrix} 2 \\ 30 \\ 2 \\ 2 \end{bmatrix}$	30	15 1 6	2		III V IV	1
3601.372 3601.899 3602.178	III	1 1 1	}	2			V		3625.739 3626.340 3626.711	II	4 1		3 10 8*			IV	
3602.823 3603.162 3603.329 3603.655 3603.755	I I I I I I I I I I I I I I I I I I I	20 10 1 2 1	(15)	3 1 20 5	6	2	IVE IV II V III	1	3626.783 3626.872 3627.127 3627.359 3627.897	I I I I I I I I I I I I I I I I I I I			15 2 1 6	3		IV IV IV IV	
3604.342 3604.482 3604.873 3605.120 3606.118 3606.385	I I I I I I I I I I I I I I I I I I I	1 4 2 150 2	100	3 5 50			IV V V IVE V	3	3628.018 3628.565 3629.418 3630.237 3630.476 3630.552	IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	3 1 100 250 10 10	80 150 (6)	3 15 8 100 4 5	3		IV IVE IVE IVE IV	$\begin{bmatrix} 3 \\ 1 \\ 1 \\ 3 \end{bmatrix}$
3606.944 3607.141 3607.688 3608.038 3608.089	I II II II	4 1 2		5 1 4*			IV V IV		3630.843 3632.776 3632.803 3633.018 3633.274	II	5 25 5 15 8	20 25	2 - 10 1	}		IV IIIE IVE IV	
3609.247 3610.795 3610.915 3610.989	I II I	8 1		1 15 10	4 2		IV V III III		3633.758 3634.322 3634.409 3634.777	II	$\left\{\begin{array}{c} 10\\ 10\\ 12\\ \end{array}\right\}$		12			IV (V) III	}3
3611.228 3611.946 3612.362 3612.780 3613.079 3613.618	I II II II II	3 3 1d 25 15 1	(35) 20	25 10 1 1 1	1		III V IVE IVE IV	1 1	3634.838 3635.267 3635.633 3635.742 3636.254 3637.275	11 11 11 11	$\left. \begin{array}{c} 30 \\ 30 \\ 1 \\ 15 \\ 20 \end{array} \right.$	(12)	5 1* 3 6	1		IVE IV IV IVE	1 3 3
3614.074 3614.702 3614.774 3614.947	II	30 } 5 } 6	(30)	30	1* 1*	V	VE IV	1	3638.535 3638.801 3638.917 3639.814	II II	$\left. \begin{array}{c} 2 \\ 2 \\ 6 \end{array} \right.$	}	3*			IV IV	2
3615.052 3615.186 3615.564 3616.078 3616.366	I II I	1 1 8 5		3			V V IV	3	3639.902 3640.248 3640.830 3641.072 3641.633	11 11 11	100 10 2 3	60	40			IVE V IV V	1
3617.203 3617.633 3617.780 3618.104	I II II	4 5 3 30	(30)	2 1 3	i i		IV IV V IVE	1	3641.830 3641.984 3642.623 3643.524	I I I	3 3		25 3 3 30	6		III IV IV III	
3618.509 3619.451 3619.975 3620.161	11 11	30 6 10 60	(12) (4) (10) 40	30 2 1 8			IVE IVE IVE	1 1 1 1	3643.923 3644.181 3644.498 3644.899	I I I I I I I I I I I I I I I I I I I	40d 1 2d 1	15	20	20	-	IVE V IV V	1
3620.544 3620.575 3621.090 3621.566	I I I I I I I I I I I I I I I I I I I			4* 12 15	1 8		IV IV V	3 3	3645.398 3545.860 3646.294 3646.612 3646.895	I I I I I I I I I I I I I I I I I I I	1000 30 1 15 3	800 20 15	100 3 3	30		IIIE IVE IV VE IV	1 1 1
3621.792 3622.045 3622.123	I	$\left. \begin{array}{c} 1 \\ 1 \end{array} \right $	1 7	$ \begin{cases} 3 \\ 15 \end{cases} $		1 3	(IV)		3647.258 3647.600	II	$\begin{vmatrix} 3 \\ 1 \\ 2d \end{vmatrix}$		10	3		V	

TABLE A. Temperature classification of dysprosium lines - Continued

Wave-	Spec-		3 - 1	Intensity			Temp.		Wave-	Spec-		I	ntensity			Temp.	
length	trum		C 1		Furnace		Class	Notes	length	trum		6 1	F	Furnace		Class	Notes
(Air)		Arc	Spark	High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low		
3647.977 3648.365 3648.459 3648.785	I II II	3 4 5 60	} 50	8 1 3	1		IV IV IVE	1	3672.300 3672.700 3672.920 3673.140	11 11	125 40 1 40	80 20 15	15 10 6 8			IVE IVE IV IVE	1 1 1
3650.052 3650.415 3651.133	II	6d		1 5			IV V		3673.768 3673.814 3674.085	I	$\left. \begin{array}{c} 2 \\ 250 \end{array} \right.$	60	1* 80			IV	1
3651.742 3651.866 3651.966	II	2		5*			ZIV	3 3	3674.452 3675.137 3675.383	I I I I I I I I I I I I I I I I I I I	8 1 1	00	4	1 12	2	IVE III V	1
3652.292 3652.828 3653.278 3653.727	I	2 2 1 2		15 1	1		IV V V		3675.569 3676.023 3676.430 3676.590	11 11 1	2 4 10d 250	60	3 5 60	,		IV V IV IVE	1
3653.874 3653.898 3654.184 3654.876	11 11	$\left.\begin{array}{c}4d\\8\\10\end{array}\right.$		1 1			IV IV		3677.042 3677.266 3678.019 3678.121	I I I	4 3 1		4 3			IV IV V IV	
3655.618 3655.907 3656.358 3656.877 3656.956	III	$\begin{cases} 6 \\ 2 \\ 3 \end{cases}$		10 1 6*	2		IV IV	3	3678.357 3678.507 3679.119 3679.273	I II II	2? 10 1 2		10 4	} 15	3	V II V	3
3657.795 3658.151 3658.502	II	2,2		1 15	4		V IV III	3	3680.613 3680.655 3680.804	II	$\left. \begin{array}{ccc} 2 \\ 2 \\ 1 \end{array} \right.$		2* 1			IV	3
3658.712 3658.943 3659.299	I I I I	2		3		T.	IV V	3	3681.038 3681.420 3681.710	II II	2 1 1					V V	3
3659.848 3660.251 3660.674 3661.080	III	$\begin{array}{c} 3 \\ 1 \\ 1 \\ 2 \end{array}$		4	1		V IV V		3681.951 3682.612 3683.089 3683.402	II II	2 2 2 10d		8	1		V IV V	
3661.235 3661.268 3661.780 3662.261	III	$\begin{cases} 3 \\ 15 \\ 2 \end{cases}$	15	2* 1 3			IV IVE IV	1	3684.400 3684.853 3685.782	I	$\begin{bmatrix} 2\\8d\\30 \end{bmatrix}$		$ \begin{cases} 1 \\ 3 \\ 12 \\ \hline 30 \end{cases} $	} 3 } 30	8	IV (IV)	
3662.851 3663.347 3663.739	II	1 1 1		8			V IV V		3686.441 3686.890	II	1		50	30	0	V	3
3664.248 3664.615 3664.680 3664.985	I I I I I I I I I I I I I I I I I I I	$\begin{cases} 1 \\ 60d \end{cases}$	50		}		V	1	3687.151 3687.440 3687.659 3688.306	I I I	1 1 1 5		2 8 4 10	1		IV IV IV	
3665.008 3665.233 3665.401 3666.031	I	$\left. \begin{array}{c} 1 \\ 30 \\ 5 \end{array} \right.$	30	5	6		VE IV	1	3688.593 3689.031 3689.300 3689.465	I II - I	3		8 5	1		IV V IV	
3666.333 3666.364	II	$\left. \left. \left. \right\} \right. \left. \left. \left. \left. \right\} \right. \right. \right. \right. $		1* 1*			IV		3689.888 3690.297 3690.361	I	$\left.\begin{array}{c} 3\\1\\2d\end{array}\right\}$		5	1		IV	
3666.839 3666.998 3668.093	III	$\begin{pmatrix} 6 \\ 3d \\ 1 \\ 2 \end{pmatrix}$		30	15	3	III V IV		3690.576 3691.236 3691.584	I I II	3 4 1		4 2			IV IV V	3 3
3668.542 3668.726 3668.903 3669.175 3669.664	1 I I I I I I I I I I I I I I I I I I I	3 2 6 1	(4)	2 3			V IVE IV V	1	3692.076 3692.260 3692.289 3692.484 3692.986	I I I II	3 3 3		8 10 1	2		V IV III IV	}
3670.515 3670.903 3671.689	I	1 1 20	15	3			IV V IVE	1	3693.531 3693.874 3693.970	I I II	1 4 2		6 20	3		IV III V	}3

Table A. Temperature classification of dysprosium lines - Continued

W/	C			Intensity			Т		W/	C		I	ntensity			Т	
Wave- length	Spec- trum		C 1		Furnace		Temp. Class	Notes	Wave- length	Spec- trum		C 1	F	urnace		Temp. Class	Notes
(Air)		Arc	Spark	High	Medium .	Low			(Air)		Arc	Spark	High	Medium	Low		<
3694.371 3694.415 3694.810 3695.658	II II II		20 300	1 60 1	5		IVE IIIE IV	1 1	3729.270 3730.606 3730.673 3731.139	II II II			10	1*		V IV	
3696.083 3696.587 3696.885	I	2		1			IV V		3731.292 3732.075	I	4 1 2)	5 3	÷.		IV IV	
3696.947	11	10d		8	1*		III		3733.336	I	3	}	8	1	8	IV	
3696.962 3697.314	I	30	20	$\left\{\begin{array}{c}2\\5\end{array}\right.$	}		IVE	1	3734.269 3734.378 3735.993	II	5d 4 2		15	2		IV V	3
3697.637 3697.958	I	3		5			IV V	3	3738.292 3738.594	II	3		60	20	10	V	
3698.207 3698.304 3698.714	II	60 ?	50	5 1 4d			VE IV IV	1	3739.344 3739.858 3740.064	III	20 5 12		60	20	10	V II	×
3698.980 3699.723	I	5 1		6 3	, %	, :	IV	3	3740.379 3740.529	II	1	}	2*			IV	
3700.577 3700.727	II	} 10		8	1*		III	3	3741.201 3741.894	I	8 15d		15	5	1	III	
3701.627 3701.903	II	40	30	3			IVE V	1	3742.350 3743.053	I	134		10	1		IV	
3703.235	I	1		15	2		III ,		3743.115	I	} 2		2	2*		II	
3704.526 3704.699	I	$\left. \right\}$ 2		6d			IV		3743.868 3744.930	I	3		4			IV	
3705.807 3705.830	II	5 2		5	1		(V)	}.	3745.497 3745.540	I	} 5		15*			IV	
3706.385 3706.798	I	$\begin{array}{c c} 1 \\ 2 \end{array}$		$\frac{1}{20}$	1		IV		3745.819 3747.817	II	100	40	20	1 ^ .		V IVE	1
3707.212 3707.404	I	1 30	20	2 5		~	IVE	1	3748.056 3748.550	II I	20	20	6			VE IV	1
3707.573 3708.220	II	20 40	(15)	15 10			IVE IVE	1 1	3748.779 3750.316	I	1	1				V	
3710.071 3710.744	II	30 10	25	3			IVE V	1	3750.346 3751.802	I I	} 15 20	15	1			VE IV	1
3711.662 3711.814	II	30	20	2 2			IVE IV	1	3752.382 3752.808	I	2 2		5 40			IV	
3713.843 3713.865	II	} 15	10	15	3*		IIIE	1	3753.506 3753.749	II	150 200	60 100	15 4			IVE IVE	1 1
3714.430	I	1	10	4			IV	1	3754.809	I	8 <i>d</i>	100	10	1		IV	1
3715.313 3716.941	II	15 20	10 20	1 1			VE VE	1	3755.137 3755.381	I	3 4		10			IV	
3717.284 3718.135	II	8		30 1	8	2	IV		3756.094		2		$\left\{egin{array}{c} 3 \ 2 \end{array} ight.$	} 1		III	
3718.691 3718.919	II	4		12			(III)		3757.054 3757.372	II	8 500	300	20 60	30 2	20	IVE	1
3719.431 3720.834	I	4 2		6 25	1 10	5	IV		3758.988 3760.086	II	5 2		1 1			IV	
3721.712 3721.809	I	2d		3 3			IV		3760.362 3760.850	I	2 1					V	
3722.672 3722.784	II	15 1		5			V		3761.407 3761.517	I	2		5 6	2		(III)	}3
3724.446 3724.891	II	150	80	50 8	1 1		IVE III	1	3762.234 3762.274	II	$\left.\right\}$ 8d		1*			IV	,
3725.441 3725.935	II	15 4		1 40	5	1	V		3762.691	ΙΙ	$\begin{cases} 10d \end{cases}$, , , , , , , , , , , , , , , , , , ,	. ,	v	
3726.178 3726.548 3727.091	I	2 3 2		20	2		V V	* 1 1 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3762.766 3764.316 3764.835	I	8 6		1 8		, ,	IV IV	
3727.999	I	$\left\{ \begin{array}{c} 5 \\ 8 \end{array} \right $	}	50	8	3	III		3765.969 3766.214	I	1 3		5 8	1 2		IV	
3728.432 3728.467	II	3 4					V		3767.628 3768.507	I I	15 1		30 1	20	8	IV	

Table A. Temperature classification of dysprosium lines - Continued

7	11/	6			Intensity			T		NV.	6		I	ntensity				
	Wave- length	Spec- trum				Furnace		Temp. Class	Notes	Wave- length	Spec- trum		0 1	F	urnace		Temp. Class	Notes
	(Air)		Arc	Spark	High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low	1	
:	3769.095 3769.370 3770.701		1 1		10 8 3	-1		IV IV IV		3825.680 3825.951 3831.641	II	30 <i>d</i> 20? 20	15 30 15	?			E E E	1 1 1
:	3771.107 3771.164	I	4 2		15 8?	6 2	2	II	, .	3836.504 3838.658	II	60	(35)	5?			IIIE	1,2
3	3772.105	I	$\begin{bmatrix} 2\\2\\2 \end{bmatrix}$		2 12	3	1	IV II		3840.894	II	5 10	(95.)	5?			VE	2 2
:	3772.642 3773.052	I	115	20	40	20	8	II	,	3841.310 3842.004	I	40 20	(25)	3 2?			IVE	1,2
3	3773.303 3773.766	I	25	20	6 4	1 1		IVE	1	3844.363 3846.342	II	15	(10)	3			VE	2,3
3	3774.843 3775.937	I	$\begin{cases} 10 \\ 2 \end{cases}$		1			IV		3847.022 3848.398	I	8 2	,	6 3			III	2 2
<u>}</u>	3776.030 3776.921	II	4					V		3849.388 3850.036	II	15 5	(15)				VE VE	1,2
3	3777.434 3779.032	I	$\frac{5d}{3}$		25?	2		V	3	3850.420 3850.515	II	4 5					VE VE	2 2
3	3779.232 3779.671	II	10 1	(8)	1 6			IVE	1	3853.027 3854.935	II	50	(35)	3			VE VE	1,2
3	3780.308 3780.944	I	3 2		20 15	4		III	v.	3855.636 3858.104	II	5 5					VE VE	2 2
3	3781.468 3782.154	I	10 1		12	6		V		3858.404 3862.700	I	15 5		8? 3			III	2 2
	5782.871 5783.595	II	10 12	(5)	4			IVE V	1	3863.245 3865.482	II	8			*		VE VE	2 2
	783.941 783.972	I	8		6	1*		IV		3866.580 3867.855	II	20 5	(15)	,			VE VE	1,2
3	784.559 785.214	I	2 2		4 2	1		III	3	3868.450 3868.808	I I	25 50	(15)	2? 12?			IVE	1,2
	785.411 786.176	II	15 300	(8) 150	100	1 5	1	IIIE	1 1	3869.137 3869.424	II	3 10	(6)	- 1			VE VE	2 1,2
	786.826 787.256	I	2 5		8	2	,	IV		3869.864 3871.628	II	25 10	(12)	?	,		VE VE	1,2 1,2
	788.436 789.850	II	150	80	80	?	_	IV	1	3872.107 3873.986	II	300 40	(250) (25)	?			IVE IVE	1,2 1,2
	789.894 791.871	II	50	25	8			IVE	1	3875.179 3877.943	I I	4 2				-	VE VE	2 2
	793.513	II	2 3					V		3879.058 3881.993	II	$\frac{20d}{12}$	(20) (10)				VE VE	1,2 1,2
	795.428 795.989	II	3		204			V		3883.066 3887.540	I I	4 8		1	,2		VE IV	2 2
3	796.048 796.817	II	$\left. igg egin{array}{ccc} 1 & & \ & 2 & \end{array} ight.$		2?* 15	4	1	IV		3888.426 3888.951	I I	6	(8)	2			VE IV	$\frac{1,2}{1^2}$
3	797.750 798.312	I	3 2		12	6	1	III		3889.013 3891.865	II	20	10	6		-	(IV)E VE	
3	798.567 799.014	I	2 2	- "	6	2		III		3891.969 3892.901	I I	6 12		5 8?		7	III II?	2 2
3	799.564 799.903	II	3		4	2		V		3893.382 3894.530	I I	1 2		6	8 1		IIIA	2 2
3	800.404 801.571	I .	$\frac{1}{2}$					V		3895.373 3896.218	II	15 1	(18)	6			VE IIIA	1,2
3	801.926 802.693	II	5 1		1			V		3896.651 3898.529	I	300	(240)	6 20			IIIA	2 1,2
3	803.549 804.142	I	1 40	20	8	2 2		III	1	3899.120 3899.169	I	6	(240)	$\left\{\begin{array}{c} 20 \\ 4 \\ 6 \end{array}\right.$			III	}2
3	804.352 805.832	I	4 1	20	3	1		IV IV		3902.400 3903.072	H	$\begin{bmatrix} 2 \\ 1 \end{bmatrix}$		U			VE (?)	2
3	806.271 807.474	11	50	100	1? ?	1		IVE ?	1	3903.072 3903.330 3904.084	I	8 2		15 8			III	
3	809.020 813.672	II	25 40	20 30	3			E E	1 1	3904.210	II	20	15	1			VE	1
3	813.672 816.762 822.580	II	200 20	150 15	10 5			E	1 1 1	3905.172 3905.598 3905.941	I II I	1 ? 3		2 1? 10			VE III	

Table A. Temperature classification of dysprosium lines - Continued

XV/	6			Intensity			T		W/	C		I	ntensity			Т	
Wave- length	Spec- trum		Spark		Furnace		Temp. Class	Notes	Wave- length (Air)	Spec- trum	Arc	Spark	F	urnace		Temp. Class	Notes
(Air)		Arc	эрагк	High	Medium	Low			(AII)		Aic	Зраг к	High	Medium	Low		
3907.573 3909.135 3910.106	I II I	$\begin{array}{c} 1 \\ 2 \\ 4d \end{array}$		4 1 12			(III) (IV) III	, ,	3949.248 3949.700 3950.389	I I I I	1 1 20	(20)	2 2 1			(III) (III) VE	
3910.547 3911.672	II	$\left\{ egin{array}{c} 2 \ 2 \ 3 \end{array} ight.$		5 5	}		VE	. ~	3951.342 3951.837 3952.135	I I I	1 1 1		1 2 3			(IV) (III) (III)	1
3912.298 3912.545	I	2 10		5 10			(III)		3952.481 3953.128	II	1 3				7	(V) (V	
3912.866 3913.062 3913.625	I	5 10		20			VE (III) III		3953.191 3953.500 3953.970	I I	4		3 6 1			(III) III (IV)	
3913.974 3914.866	II	5 40	(7) (20)	3			VE IVE	1 1	3954.552 3955.100	II	20 2	(15)	2			VE (IV)	1
3915.594 3917.292 3917.376	I	40 30 20	(20)	4 30 15			IVE	1	3955.353 3955.484 3956.252	I II I	1 1 2	7 - 5	1 4	* 2 2	å , ,	(IV) (V) (III)	
3917.985 3918.555	I	1 6		1			(IV) VE		3956.809 3957.240	I I	3	(20)				(V) (V)	
3919.125 3919.156 3920.114	I	$\left \begin{array}{cc} 5d \\ 2 \end{array} \right $		{ 5 15 5			(III) III	-	3957.790 3957.996 3958.832	I I	30 2 1	(30)	1 4			VE III (V)	1
3920.860 3921.313	I	4 1		6 2 5			(III)		3959.380 3959.700	II	4 2 1					VE (V) (V)	
3922.049 3922.617 3923.291	II	2 2 3		3			(III) (V) VE		3960.827 3961.802 3962.152	I	5		5 1*			(IV)	3
3923.380 3924.409 3924.466	I	10 4 3	(10)	(6?)			VE IIIA VE	1 2	3962.454 3962.590 3962.791	I I I	$\left.\begin{array}{c} 1\\ 10\\ 2\end{array}\right.$,	8 2			III (IV)	
3925.261 3925.563	I	$\frac{3}{1}$		3	2		(III)	3	3963.165 3963.807	I	3 4		4			(III) VE)
3926.771 3927.300 3927.861	III	2 1 10		3			(III) (V) III		3964.712 3965.155 3966.356	II	3 1 5		2			VE (III) III)
3928.005 3929.333	II	3 5	(7)	0			V VE	1	3967.512 3968.391	I	$\begin{array}{c} 10 \\ 1000 \end{array}$	800	10 20			III	E 1,
3929.716 3930.146 3931.281	II	2 15 8	(6)	8 2			(V) III IVE	1	3969.227 3971.214 3971.613	I I I	10 8 2		5 10 3			III (III)	
3931.524 3932.078	II	150 3	125	5			IVE (V)	1	3972.415 3973.313	I I	4	,	6 1			(IV)	
3932.216 3932.995 3934.207	II	10 6 8	(10)				VE VE VE	1 1	3973.877 3975.075 3976.962	I I I	12 2 2		10 5 4			(III) (III))
3934.373 3936.054	I	3 5	(5)	5			(III) VE	1	3978.566 3979.471	II	250 10	200 (6)	5 2			IVE VE (III	1 1
3936.295 3936.700 3937.164	I	4 10 4	,	8 5			VE III III		3979.945 3980.369 3980.695	I I I	2 1 1		4 1 1			(IV)	
3937.984 3938.046 3938.203	I	3 4 6	7	5		ı	VE	\$	3981.366 3981.924 3982.512	I	$\begin{array}{c} 3\\100\\2\end{array}$	80	20 2 ?			III IVE (?)	1
3938.842 3939.260	I	1 1		1 3			IV IV		3982.843 3983.652	I I II	1 100	(70)	1 4	-		(IV)	1
3939.794 3942.045 3942.527	II	2 3 25	(20)	6			IV VE VE	1	3984.210 3984.691	11	60	(40)	1			IVE VE	1
3944.683 3945.634	II	600	(450)	50			IIIE (V)		3985.356 3986.059 3987.070	I I	2 4		6			III VE	
3945.913 3946.343 3946.929	I	3 2 15	(20)	4 5			IV (III) VE	1	3987.541 3988.207	I I	3 1 2		2			(III)	1

 ${\it Table A.} \ \ {\it Temperature classification of dysprosium lines-Continued}$

Wave-	Spec-			Intensity			Temp.		Wave-	Spec-		Iı	ntensity		× .	Temp.	
length	trum		G 1		Furnace		Class	Notes	length	trum			ŀ	Furnace		Class	Notes
(Air)		Arc	Spark	High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low		
3988.880	I)						. 1,	4024.899	I	8		6			III	
3988.931	I	$\left.\right\}$ 6d		5?			III		4025.391	I	2		4	-		III	3
3989.683	I	2		5			(III)		4025.603	I	4		4	,		III	
3990.336	11	3					VE		4026.054	I	1		2			(III)	3
3990.734	I	1		1			(IV)		4026.754	I	1		2			(III)	3
3991.316	ΙI	30	25				VE	1	4027.779	11	15	(12)				VE	1
3991.849	ΙΙ	3					VE		4028.316	11	8					VE	
3992.457	I	1		1		,	IV		4028.412	I	12		10			II	
3993.274	II	1					VE		4031.075	I	3	(20.)	8			III	,
3993.571	I	8		$\frac{6}{2}$			(III)		4032.471	II	30 4	(30)	$\frac{1}{2}$			VE III	1
3993.680 3993.854	I	1		3			III		4032.540	I	1		$\frac{2}{2}$			III	
3993.634	I	4		6			III		4033.655	II	10					VE	
3995.333	I	1		1			(IV)		4036.325	II	15					VE	
3995.757	II	3		•			(V)		4037.624	I	3		2			III	1
3995.990	I	5		8			III		4038.512	11	8					VE	
3996.688	11	150	100	4			IVE	1	4038.708	I	1		5			III	
3996.920	I	2		5	,		III		4038.828	I	4		3			III	
3998.060	11	3				0.	VE		4040.771	I	2		3	1		(III)	
3998.204	I	2		4			(III)		4041.975	ΙΙ	10					VE	
3998.938	I	1		5			III		4043.035	I	1	· ·	3			IIIA	2
3999.847	ΙΙ	2					(V)		4043.388	II	2d	1				(V)	
4000.450	H	800	600	10			IIIE	1	4045.271	I	2		4	-		III	
4000.589	I	1		4			III		4045.971	I	400		200			II	
4001.188 4001.521	I	$\begin{bmatrix} 1 \\ 2 \end{bmatrix}$		$\frac{1}{4}$			(IV)		4047.391	II	3		2			(V)	
4001.321	I	1		3	. ,		(III)		4048.377	II	3d?		2			(V)	
4004.297	I	$\frac{1}{3}$		5		*	(III)		4048.931	I	54.		5			III	
4004.452	I	1		2			III		4049.362	I	5		8			II	
4005.838	I	12		8			III	,	4050.564	11	150	(90)	3			IVE	1
4006.071	I	10		8			III		4052.448	I	1	` ′	3		,	III	
4006.444	I	2		6			(III)	3	4054.988	I	8	-	5			III	
4006.738	11	4					(V)		4055.144	ΙΙ	30	(20)				VE	1
4007.136	I	4		6			III		4057.373	ΙΙ	} 3					VE	
4007.759	II	6		_			VE		4057.441	ΙΙ	J		,				
4008.478	I	2	1	5			(III)		4058.159	I	2		1			(IV)	
4009.330 4009.855	I	$\begin{array}{c c} 1 \\ 3 \end{array}$		3 5)	(III)		4060.566	II	$\frac{5}{2}$		3			VE	
4010.067	I	5		3			VE		4065.158	I	$\frac{2}{2}$		2			III	
4011.161	I			1			(III)		4065.391	I	4		5			III	
4011.288	II	20	(15)				VE	1	4066.745	I.	2		4			III	
4011.816	I	1	(/	2			III		4067.960	I	2		4			III	
4012.524	I	2		5		-	III		4071.021	I	3		4			III	
4012.816	11	2d					(V)		4072.609	ΙI	3	* .				VE	
4013.826	I	15		40r			II		4073.116	ΙΙ	150	80	10			IVE	1
4014.097	I	1		6			III	- 1	4073.985	ΙΙ	3					VE	100
4014.704	II	20	(12)	1			VE	1	4077.340	I	2	500	3			IV	
4015.172	II	4				-	VE	2	4077.964	H	800	500	20			IIIE	
4016.748	I	} 2		1*			(IV)	3	4079.258 4079.586	I	3		5 5			III	
4016.895 4017.054	II	3		5			III		4079.380	I	, 3		3			III	
4017.752	I	$\begin{array}{c c} 3 \\ 1 \end{array}$		3			(V)		4081.835	I I I	2		2*			(IV)	
4018.476	I	1		1			(IV)		4033.100	I	4		6			III	
4019.396	II	$\frac{1}{2}$					VE		4083.802	I	2	1	4			III	
4019.548	II	2					VE		4085.130	I	15		15			III	1
4020.032	I	1	,	1			(IV)		4085.336	I	20		20			III	
4020.868	ΙI	5					VE		4087.199	ΙI	15	(12)		1.		VE	1
4020.897	I	1		5			III	4 7	4087.381	I	5		6	- 2 -		III	
4022.554	I	1.		2			(III)		4089.502	I	3		5			III	
4023.587	I	2	,	5			(III)		4090.389	I	1		3		1	III	
4023.713	I	10		15		1476	III		4091.520	H	10	(8)				VE	1
4024.428	II	10					VE		4091.759	II	6			1		VE	

TABLE A. Temperature classification of dysprosium lines - Continued

TV /	6		1	ntensity			т		W	c.		I	ntensity			T	
Wave- length	Spec- trum				Furnace		Temp. Class	Notes	Wave- length	Spec- trum		C 1	F	`urnace		Temp. Class	Notes
(Air)		Arc	Spark	High	Medium .	Low			(Air)		Are	Spark	High	Medium	Low		
4093.638	I	3		5			III		4159.313	I	8		8			III	
4095.244	I	1		3			III		4160.247	I	3		3			III	
4096.099	I	20		15			III		4162.246	I	4		4			III	
4096.624	I	$\left\{ \begin{array}{c} 2 \\ 2 \end{array} \right.$	}	5			III		4164.732 4166.234	I	3 4		4 3			III	
4099.880	I	4		10			II		4167.225	II	2	1	3				
4101.393	Î	2		4	8-		III		4167.552	II	2	}				(VE)	3
4101.840	I	1		3			III		4167.974	I	400		100R	7		II	
4101.933	II	2					VE	_	4169.043	I	. 3		5			III	
4103.304	II	600	400	150	-		IVE	1	4169.247	II	5 2		5			VE III	
4103.874 4105.017	I	60		6? 5			III		4170.317 4170.562	I	3		4			IV	
4105.035	II	8	(6)	, ,			VE	1	4171.930	I	6		8			III	
4105.256	I	3					(V)		4172.002	I	8		8			III	
4105.804	I	2		3	*		III	· .	4176.601	I	4		3			III	
4105.988	I	2	,	2			(III)		4176.784	I	3		3			III	
4106.378	II	5					VE		4177.766	I	3		3	*		III	
4106.679	II	3					VE		4178.086 4181.269	I	6 3		4 5			III	
4107.170 4107.359	II	2 3					(V) VE	3	4182.404	11	3		3			VE	
4107.337	I	1		1			(III)		4183.599	I	8		10?			III	
4111.343	II	150	(100)	40		-	VE	1	4183.723	I	30		30 r			II	
4113.054	I	5		8			III		4186.818	I	600		300R			II	
4114.052	II	} 4d				12	VE		4189.396	I	3		4			III	
4114.117	II)							4190.939	I	10		8			III	
4114.642 4119.310	I	$\frac{3}{10}$	(8?)	6			IV VE	1	4191.642	I	100 500	1.	50R			II	
4119.510	I	10	(0:)	4			III	1	4194.845 4195.254	I	8		200R			III	
4124.626	11	20	(10)	2			IVE	1	4198.019	I	25		15			II	3
4126.086	I	8		151			II		4201.027	I	3		5			III	
4128.238	II	20	(10)	1			IVE	1	4201.304	I	15		15			III	
4129.117	I	10	50	15r			II	,	4201.372	II	10		00			VE	
4129.422 4130.351	II	100 10	50	$\frac{3}{12r}$			IVE	$\begin{vmatrix} 1\\2,3 \end{vmatrix}$	4202.241 4204.001	I	20 2		20 r 4			III	
4131.021	II	6		121			VE	2,0	4205.062	I	15		10			III	
4132.835	II	3					VE		4206.542	11	30	(15)	6	1		IVE	1
4133.353	11	6					VE		4207.696	I	6	-	6			III	
4133.849	I	15		8			III		4211.239	I	15		30 r			II	
4134.146	I	10		4			III		4211.715	I	1200		600 <i>R</i> 50 <i>R</i>			II II	
4134.708 4136.901	I	4		4			IV		4213.179 4214.410	I	5		12			III	
4137.349	II	4					(V)	7	4215.159	I	80		100R			II	
4138.539	I	4		6			III		4216.985	I	2		4	7 -		III	
4139.558	I	4		6			III		4218.091	I	200		150R	* *		II	
4141.385	I	3	(0)	6			III	١,	4218.574	ΙΙ	4		200			VE	
4141.505	II	300	(8)	2 5			IVE	1 1	4221.108 4222.210	I	250		200r 15			III	
4143.099 4145.621	II	2	(100)	3			VE	2	4224.672	I	3		4			III	
4146.060	I	100		30 r			II	_	4225.155	I	150		100 r			II	
4147.968	I	3		4			III		4232.024	I	30		15			II	
4148.957	I	2		4			(III)		4234.132	I	3		4			III	
4149.776	I	2		4			III	3	4234.831	I	5		4			III	1
4152.424 4153.122	II	8 5		4			VE		4236.264	I	2		4			III	1 1
4153.122	I	4		5		1	III		4236.579	I	1		4			III	1
4154.202	II	5		J			VE	- 1	4237.523 4237.945	II	3		9			VE	
4154.242	I	3		4.			III		4237.945	I	2		3	8		VE	
4154.515	I	3		4			III		4238.455	II	3					VE	
4156.361	I	4		3			III		4239.852	I	40		30 r			II	
4156.952 4157.862	I	5 4		6			VE		4240.685	I	1		$\frac{30r}{2}$			III	
	II	4				1	I V M.		TATU.UUJ	1	1	1					1

Table A. Temperature classification of dysprosium lines - Continued

XV/	C-			Intensity			Т.		Wave-	Spec-		I	ntensity			Temp.	
Wave- length	Spec- trum		C I		Furnace		Temp. Class	Notes	length	Spec- trum	A	CI-	ŀ	Furnace		Class	Note
(Air)		Arc	Spark	High	Medium	Low			(Air)	, L	Arc	Spark	High	Medium	Low		
4241.818	I	1		5			III		4302.581	II	12					VE	
4242.716	I	3		4			III		4302.714	II	8					VE	
4242.990	I	3		4			III		4306.766	I	1		3			III	
4243.435	I	5		10			III		4308.349	I	2		5			IIIA	A 2
4244.792	II	2					VE		4308.626	11	200	100	8			IVE	1
4245.912	I	30		20			III		4311.946	I	2		4			III	
4247.345	II	10	(8)				VE	1 .	4312.431	I	1		4			III	
4248.451	II	3	(0)				VE		4313.880	11	2					VE	
4248.893	I	1		2			III		4313.931	I	6		6			III	
4250.337	I	3		3			III		4315.603	I	1		4			III	
4250.459	I	2		5		2	III		4318.356	I	1		4			III	
4251.319	I	3		8			III		4318.991	I	6		4			III	
4251.733	I	5		6			III		4322.184	11	5					VE	
4252.122		1		3			III		4322.367	I	1		4			III	
4254.923	I	1		3			III		4322.533	11	8					VE	
4255.955	II	2					VE		4323.795	I	4		5			III	
4256.205	II	5					VE	_	4324.661	11	1					VE	
4256.330	II	15	(5)	3			IVE	1	4325.108	ΙΙ	20	(15)				VE	1
4257.698	- 11	1	()				VE		4326.375	I	15		4			III	
4257.785	I	1		10			III		4328.668	I	1		2			III	
4258.149	I	5		10			III		4328.902	ΙΙ	15	(8)				VE	1
4258.514	I	1		5			III		4329.886	11	$\int 2$	}				VE	
4258.577	I	10		10			III		4329.000	11	3	ſ				V.D.	1
4259.768	I	1		3			III		4334.052	I	1		3			III	
4259.831	I	1		3			III		4334.358	I	1		6	92		III	
4260.715		1		2			III		4335.995	I	1		6			III	
4264.834	I	1		2			III		4338.459	I	2		1			(IV)	
4265.789	II	2					VE	-	4339.622	ΙI	200	(25)				VE	1
4266.007	I	. 1	- 1	4			III		4339.654	II	} 20	(23)					1
4267.870	I	4		3			IV		4340.407	II	2					VE	
4268.264	I	5		10			III		4346.371	ΙI	10					(VE)	2
4269.545	I	6		8			III		4347.708	I	15		6			III	
4272.976	I	3		4			III		4356.109	I	2		6			III	
4273.133	II	. 5					VE		4356.747	I	3		3			III	
4274.954	I	4		6			III		4358.443	ΙI	40	(15)	2			IVE	1
4275.405	I	3		3	, ,	- 1	III		4360.186	ΙI	6					(V)	
4275.918	I	1		3			III		4361.343	II	8					VE	
4276.688	I	15		15			III		4364.046	II	5					VE	
4277.715	I	1		3			III		4364.204	ΙΙ	15	(20)			× 1	VE	1
4279.730	I	6		8			III		4365.612	I	2		11		100	III	
4282.057	I	1		3			III	1.51.	4366.722	I	8		12	1 1		III	
4283.259	I	1		5			III		4368.256	I	1		2			III	
4283.575	I	2	1 I	5			III	1	4369.541	I	2	(10)	6			III	
4284.232	I	1		3			III		4374.235	H	40	(12)	3			IVE	1
4288.019	I	1	W 5 1 - 1 5	3			III		4374.764	II	30	(20)	2			IVE	1
4288.185	I	1		2		, ,	III	×. ,	4375.308	H	10	(12)		**		VE	1
4288.719	I	2		3			III	, v *	4379.338	I	2		2			(III)) 3
4290.442	I	5		8	1.75		III	*	4380.221	H	6		_			VE	
4290.952	II	1	10.0	3			III	-	4380.469	I	2		5			III	1.0
4291.955	I	8		15			III		4384.295	II	8					VE	
4294.456	I	1		2		1 2 1	III		4385.272	II	5			- 1		VE	
4294.928	H	10	(10)		1		VE	1	4389.774	I	5		3			IV	1
4295.036	I	25		8			III		4390.306	I	1		2			III	1
4296.353	I	1		3			III		4390.926	I	2		5			III	
4297.775	I	1	3, , , 5,	3			III		4393.265	I	1		3			III	,
4298.518	I	5		3			III		4394.978	II	15	(6)	5			VE	1
4298.910	I	2		5			III		4397.490	I	1		4			III	
4300.380		3		J			VE	27.19	4399.713	I	2d?		4	2		III	1
	II		4 1 4 1	4			III	1 8	4400.077	II	6					VE	136
4300.634	II	1	4.97	4	1.47				4403.957	I	1		4			III	2
4300.736	II	3	077	2		13 11	VE		4408.034 4409.378	II	10 100	(50)	5	1		IVE	

TABLE A. Temperature classification of dysprosium lines - Continued

W/	e			Intensity			Т		Wave-	Space		I	ntensity			Temp.	
Wave- length	Spec- trum		Spark		Furnace		Temp. Class	Notes	length (Air)	Spec- trum	Arc	Spark	F	urnace		Class	Note
(Air)		Arc	эрагк	High	Medium	Low			(All)		Aic	Эрагк	High	Medium	Low		
4409.909	I	1		2			III		4556.439	11	4	yle se				VE	
4411.353	I	3		3			IV	,	4557.324	I	2		4			III	
4411.669	I	1		3			III		4559.582	I	3		3			III	
4414.172	I	1		3			III		4565.091	I	50		20 r			II	
4418.095	II	5			3 15		(V)	4.0	4565.937	I	1		5			III	1
4421.683	II	4					VE	100	4566.216	I	6		3			IV	
4426.866	I	5	1	3			III		4567.044	I	5		8			III	
4430.991	II	15					VE		4568.415	I	3		3			III	
4435.774	II	3					VE	1	4573.850	II	20					VE	
4436.627	II	3		10			VE		4576.584	II	25		40R			VE II	
4444.576	I	25 20		12			VE		4577.776 4585.703	I	200		5			III	
4448.185 4449.130	II	10					VE		4585.959	I	3		4			III	
4449.702	II	200	(100)	8	1 3		IVE	1	4586.184	111	3		3			III	
4454.332	I	200	(100)	4	1 1		III	1	4586.620	-11	10		1			IV	
4455.598	II	20					VE		4587.906	11	40	30				VE	1
4467.870	II	6	(5)				VE	1	4589.088	I			12			III	
4468.137	II	30	(10)	3	1		IVE	1	4589.355	I	400d		150R			II	
4479.464	I	5					(V)		4590.553	I	5		3		, ,	III	
4480.680	I	8		10			III		4591.658	I	2		3			III	
4481.956	II	5					(V)		4591.776	II	12					VE	
4482.290	I	} 5		2*			IV		4595.127	II	5					VE	
4482.316	II)							4599.845	I	8d		6			IV	
4484.357	I	10		10			III		4601.550	I	1		4 4			IV	
4486.222 4487.857	II	5		2			(V)		4602.513 4604.298	I	3 4	2	1			IV	
4492.144	I	1		5			III		4606.037	I	10		10			IV	
4493.091	I	5					(V)		4611.692	II	1		10			VE	
4496.361	I	2		2			IV		4612.258	I	300		100			II	
4499.259	I	3		2			III	11	4613.827	I	6		6			IV	
4502.602	II	10		· .			(V)		4614.822	I	10		10			IV	
4503.232	II	50	(30)				VE	1	4615.564	II	5					VE	5-4
4503.372	I	1	(00)	4			III	1	4616.929	I	1	9	2			IV	
4505.622	II	5					(V)		4617.264	II	30	20		T A		VE	1
4506.063	11	4					(V)		4618.719	II	1	40	,			VE	1
4506.939	II	8		2			IV		4620.034 4620.378	II	60	40	1			VE VE?	1
4508.086	I	?		3			IV		4620.969	I	2		2			IV	
4513.586	I	4		12			III		4621.411	II	3		_			VE	
4516.838	I)					111		4622.370	II	5	-				VE	
4516.952	II	20		5*			III		4622.732	I	1		5	1		III	
4518.506		3	(6)				VE	1	4624.118	I	6		6			IV	
4519.815	II	10	(0)			-	VE		4624.439	ΙI	4					VE	
4522.704	I	1		4			III	12.1	4625.661	I	1-		3			IV	
4523.075	I	2		3			(III)		4626.021	I	2		1			IV	
4525.110	I	4		3			IV		4627.394	I	1		10			IV	3
4526.083	I	4		3			IV		4628.066 4631.489	II	5		12			VE	
4527.761	11	10?		3	6		VE	1	4634.762	I	10 2		2			IV	
4531.552	I	50?	,	15			II		4635.292 4637.126	I	5 6		5 3			III	
4531.532	111	$\begin{vmatrix} 3 \\ 20 \end{vmatrix}$	15	3			VE	1	4637.579	II	4		3			VE	
4539.134	II	3	15	6			IV	1	4638.800	II	5					VE	
4539.134	11	30	40	U			VE	1	4641.072	I	2		6			III	
4545.322			40				VE	1	4642.205	I)						
	II	6		9			IV		4642.237	I	} 1		3			IV	
4546.424	I	2	1.7	2				3	4642.767	II	2					VE	
4546.760	I	1	(2)	3			III	3	4643.438	I	6		3			IV	
4550.866	II	2	(3)	1		1	VE	1	4644.105	ΙΙ	1					VE	
4553.130 4555.007	I	4		8			III		4646.714	I	3		2			IV	
4000.007	I	3		4			III		4647.281	II	} 4		4*			IV	

 ${\it Table A.} \quad {\it Temperature \ classification \ of \ dysprosium \ lines-Continued}$

Furnace Class Notes Indicate Class Indicate Class Notes Indicate Class Indicate Class Indicate Indicat	Temp. Class	Notes
High Medium Low WE A723,916 1 5 1 3 3 3 4 4 4 4 4 4 4		
4653, 406	III IV VE	3
465,880	IV IV	
469.500	VE VE	1
4661,916	III	
4662.146	IV VE	1
VE	IV	1
4664.659	IV?	
466.5893	IV? IV	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	IV	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	IV IV	**
4668.162	VE	
1	III	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	VE IV	1
4672.471	IV	
4673.596	VE	1
4674.598	VE IV	1
4679.061	IV	3
4680.175	VE	1
1	IV IV	
4681.863 I 4 4 4 4764.652 I 2 3 4682.028 II 8 VE 4765.585 II 1	VE	
VE	VE IV	3
4683.775 II 6 VE 4767.151 II 2 4685.986 I 1 1 40 50 VE 1 4769.622 II 6 4690.243 I 2 2 IV 4770.798 II 1 1 4691.596 I I 1 IV 4772.444 I 1 1 4693.659 II 2 2 VE 4774.286 II 2d 4693.956 I I I IV 4774.804 I 6 3 4694.336 II A 6* IV 4775.789 I 30 20 4695.240 II 8 VE 4778.813 I I I I 4697.169 II I VE 3 4780.145 I I I	IV	,5
4689.751 II 40 50 VE 1 4770.798 II 1 4690.243 I 2 2 IV 4771.937 I 20 15 4691.596 I 1 1 IV 4772.444 I 1 1 4692.728 I 2 2 IV 4773.151 II 1 4693.659 II 2 VE 4774.286 II 2d 4693.956 I 1 1 IV 4774.804 I 6 3 4694.336 II 3 4775.789 I 30 20 4695.240 II 8 VE 4778.813 I 1 I 4697.169 II 1 VE 3 4780.145 I 1 1	VE	
4690.243 I 2 2 IV 4771.937 I 20 15 4691.596 I I I IV 4772.444 I I I 4692.728 I 2 2 IV 4773.151 II I I 4693.659 II 2 VE 4774.286 II 2d 2d 4693.956 I I I IV 4774.804 I 6 3 4694.336 II 4 6* IV 4775.789 I 30 20 4695.240 II 8 VE 4778.813 I I I 4697.169 II I VE 3 4780.145 I I I	VE VE	
4692.728 I 2 2 IV 4773.151 II 1 4693.659 II 2 VE 4774.286 II 2d 4693.956 I 1 IV 4774.804 I 6 3 4694.336 II 4 6* IV 4775.789 I 30 20 4695.240 II 8 VE 4778.813 I 1 1 4697.169 II 1 VE 3 4780.145 I 1 1	III	
4693.659 I I 2 4693.956 I 1 4694.336 I I 4694.389 I 4695.240 I I 8 VE 4697.169 I I 1 VE 4774.286 I I 4775.789 I 30 20 4776.841 I I 4778.813 I 1 I VE 3 4780.145 I 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 2 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4	IV	1 1
4693.956 I 1 1 1V 4774.804 I 6 3 4694.336 II 4 6* IV 4775.789 I 30 20 4694.389 I 5 4776.841 II 1 1 4695.240 II 8 VE 4778.813 I 1 1 4697.169 II 1 VE 3 4780.145 I 1 1	VE VE	
4694.389 I	IV	1 1
VE 4778.813 I 1 1 4697.169 II 1 1 VE 3 4780.145 I 1 1 1 1 1 1 1 1 1	III VE	
107.1120	IV	11/19
4698.684 11 60 60?	IV	
10701001	VE IV	
**************************************	IV	
4705.727 1 1 1 4705.905 - 4	VE	
4/00.7/3 1 5 6 1 1 2 4796.941 11 9	IV VE	
4700 292 11 5d	VE	1
4711 065 1 9 92 TV 4708.393 1 1 131 132	IV? IV	
4711.595 II 2 2? IV	IV	
4712.505 II 2 1	III	
777.720 1 2	IV	
1172.000	IV	
	IV	11.
	VE IV	

TABLE A. Temperature classification of dysprosium lines - Continued

NV.	6			Intensity			Т		W/-	C		I	ntensity		-	T	
Wave- length	Spec- trum		C 1		Furnace		Temp. Class	Notes	Wave- length	Spec- trum	Arc	Spark	F	Furnace		Temp. Class	Notes
(Air)		Arc	Spark	High	Medium	Low			(Air)		Aic	Эрагк	High	Medium	Low		
4800.639	ı	6		6			IV		4875.927	I	3		1			IV	
4802.142	11	1					VE		4877.115	I	1		1	3		IV	3
4804.512	I	5		5			IV		4879.170	I	1		1		×	IV	
4806.950	I	1		8			?		4880.161	I	30		30			II	
4807.942	I	12		15			III		4881.981	II	3d					VE	
4808.739	I	2		2			IV		4884.152	I	3		10			III	
4810.276	I	3		3			IV	=	4884.551	I	6		3			IV	
4810.802	ΙΙ	1		1			IV		4886.144	I	2		2			IV	
4812.801	I	8		30			III		4888.081	I	40		60			III	
4814.150	I	1		12			III	3	4889.327	II	50	60	4			VE	1
4816.517	I	1		2			IV		4889.783	II	1		_			VE	
4817.069	I	1		1			IV		4890.102	II	60	15	1			VE	1
4817.464	I	1		1			IV	, ,	4892.592	II	2					VE	
4818.203	I	.2		8			IV		4893.676	I	8		6			IV	
4819.041	I	10		10	700		III		4895.850	I	5		6			IV	
4820.275	I	1		2			IV		4897.121	II	2		٠,			VE	
4821.293	I	5		4			IV		4899.245 4901.941	I	5 6d?		3 25			IV	
4821.907	I	1		1 8			IV		4901.941	I	1		5			IV	
4823.723	I	2		6			IV IV		4905.062	I	5		30	^ .		III	
4824.964 4826.555	I	12 5		0			VE		4900.232	I	2		2			IV	
4828.880	II	8		6			IV		4909.003	H	1					VE	
4829.130	II	2		0			VE		4909.799	I	2					VE	
4829.682	II	20	20				VE	1	4911.167	I	1		5			IV	
4830.879	II	1	20				VE	1	4911.480	II	1			-		VE	
4832.377	I	15		15			IV		4912.547	II	2					VE	
4833.754	II	15	15	10			VE	1	4914.729	I	5		40			III	
4836.947	I	1	10	2			IV	1	4916.409	I	15		6			IV	
4837.683	I	2d	/	1			IV		4917.175	I	3		20			III	
4839.677	I	1		1			IV		4918.242	I	5		5			IV	
4840.169	I	1					VE		4919.554	I	1		1			IV	
4040 461		10					(IV		4921.492	I	2		2			IV	
4840.461	II	10		8			(VE		4922.221	II	25	50				VE	1
4841.082	I	1		3	1		IV	**	4923.160	II	60	25				VE	1
4841.752	I	8		3			IV		4927.332	II	2					VE	
4842.192	I	1		1			IV		4929.322	II	2					VE	
4843.422	ΙΙ	2					VE		4931.031	I	3		3			IV	
4843.767	I	1					VE		4932.474	I	1		1			IV	
4844.824	II	1					VE	,	4933.028	I	1		2			IV	3
4845.778	I	2d		4			IV	3	4933.845	ΙΙ	8					VE	
4850.952	I	1		3			IV		4936.108	I	2		2			IV	
4851.435	I	2		2			IV		4936.832 4940.425	I	1		l 10			IV	
4852.517 4854.978	I	2		2			IV		4940.425	I	$\frac{1}{2}$		10			IV IV	
4855.136	I	} 1		3d			IV	3	4942.849	I	2		3			IV	
4855.578	I	2		2			IV	3	4945.502	II	1		3			VE	
4856.239	111	20	20				VE	1	4946.262	111	4					VE	
4857.373	I	1	20	1			IV	3	4948.217	I	3		4		-	IV	
4858.971	I	1		15			III	"	4949.319	I	1		2			IV	3
4859.150	I	1		10			VE		4951.016	I	2		1			IV	
4860.051	I	1		1			IV		4951.431	I	2		3			IV	
4861.701	I)							4953.366	I	1		3			IV	
4861.798	ı	} 1		1			IV		4954.349	11	2					VE	
4865.682	I	2		1			IV		4957.338	II	1500	500	50	Y		IVE	1
4867.756	I	1		1			IV		4959.587	I	6		5			IV	
4868.050	II	15	15				VE	1	4961.742	I	1		8			IV	3
4868.650	I)		9					4963.081	II	2					VE	
4868.832	I	1		2			IV	3	4964.659	I	1					VE	
4869.660	I	1		1			IV		4969.859	I	2d?		10			IV	
4872.476	I	1		, 1			IV		4971.768	I	4		3			IV	
4873.159	I	3		3			IV		4973.568	I	6		6			IV	
4875.460	II	(?)			1		VE		4974.990	II	6	(8)				VE	1

TABLE A. Temperature classification of dysprosium lines - Continued

TV /	6			Intensity			т		Wave-	C		I	ntensity			т	
Wave- length	Spec- trum		CI		Furnace		Temp. Class	Notes	length	Spec- trum	A	Spark	F	Turnace		Temp. Class	Notes
(Air)		Arc	Spark	High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low		
4976.444	I	1		1			IV		5065.760	I	3		1			IV	
4980.126	I	2		?			IV		5067.157	1	1		-			VE	
4981.964	I	1		1			IV	0 3	5070.678	I	60		80			III	
4983.818	I	1		ī			IV	3	5071.761	I	1		2			IV	
4984.622	I	1					VE	3	5072.954	11	1				,	VE	3
4985.068	I	2		2			IV	3	5073.809	I	1		1			IV	
4985.523	I	10		6			IV		5074.274	I	2					VE	
4988.112	I	1d?		3			IV		5077.669	I	60		80			II	
4991.819	I	1		1			IV		5080.172	11	4					VE	
4993.518	I	2		8			IV		5084.947	·I	2		?			IV	
4994.808	I	3		2			IV		5086.864	I	2					VE	
4995.359	ΙI	8					VE		5088.419	11	5		_			VE	
4996.771	I	1 <i>d</i> ?		4			IV		5090.386	H	50	25	1			VE	1
4997.630	I I	1		3			IV	3	5092.203	ΙΙ	8	(8)				VE	1
4998.462	I	3	,	10			IV		5099.844	ΙΙ	2		109			VE	
4998.976	II	} 4d?	{	,			VE		5102.350	I	4		10?			IV	
4999.048		,	(1			IV		5105.331	I	2		5			IV VE	2.5
5000.108		1		_			VE		5106.347	I	8 5		8			IV	
5000.925	I	$\frac{1d}{20}$		-5 25			IV		5106.882 5107.983	I	20	20	0			VE	1
5003.867	I	50		23			IV VE		5107.965	II	20	20	4			IV	1
5004.285 5005.888	II	1		. 1			IV		5110.321	I	15		8			IV	
5005.666	I	8		. 1			VE		5110.321	I	13		15			III	
5007.415	I	1		4			IV		5113.415	II	3		10			VE	
5010.606	I	4		3			IV		5120.036	I	100		80			III	
5011.529	I	i		1			IV		5122.408	I	4		?			IV	
5012.156	I	2d		2			IV		5123.119	I	3		2			IV	
5012.579	I	1		6			IV		5125.534	I	2d?		?			IV	3
5017.986	11	10	(8)				VE	1	5127.487	I	3					VE	
5019.319	I	1					VE		5128.292	I	5		?			IV	
5021.835	I	1		30			III		5129.846	ΙΙ	15	15				VE	1
5022.118	I	50		80			III	× 4	5130.336	I	2		?			IV	
5024.032	I	5		6			IV		5131.068	ΙΙ	} 4d	{				VE	3
5024.536	I	6		25			III		5131.121	I	μ	(1			IV	3
5027.874	I	6		6			IV		5131.928	I	2		3			IV.	-
5029.233	II	3					VE		5132.221	I	2					VE	
5032.660	I	5		6			IV		5133.603	I	1		20			V	3
5032.996	I	6		6			IV		5135.023 5136.292	I	15 8		30			III VE	
5034.3 5 3 5036.9 0 1	I	$\begin{array}{c c} & 1d \\ & 1 \end{array}$		2 1			IV		5130.292	II	200	80	6			IVE	1
5037.702	I	$\frac{1}{1d}$		6			IV		5141.524	I	200	00	0			TAR	3
5039.046	I	3		15			III		5141.652	I	2d		8			IV	
5040.529	II	2		10			VE		5145.212	11	15	20				VE	-1
5042.038	I	2		1			IV		5146.978	I	2		8			IV	
5042.634	I	100		100			III		5147.192	I	3		3?			IV	
5043.624	I	2		3			IV		5148.976	I	2		?			IV	
5045.498		1		1			IV		5149.642	I	1		2			IV	
5046.300	ΙI	4					VE		5150.137	I	6d?			F.,		VE	
5047.249	I	8		20		1	III		5151.299	I	1					VE	
5049.521	I	2d		4?			IV		5151.607	I	2		4			IV	
5050.215	I	10		6		,	IV		5154.582	I	1		2			IV	
5051.241	I	1		1		-	IV		5155.305	I	60		30			IV	1
5052.010	I	4		10			IV		5156.031	I	1		4			IV	3
5053.189	I	2		_			V		5156.805	I	3		4?			IV	3
5053.352	I	5		5	1.		IV	3	5157.805 5158.917	I	1 4					IV VE	
5055.462	I	4		3			IV		5158.917	II	6		25			III	
5055.859	I	1		2			IV		5161.027	II	25	25	20			VE	1
5056.180	II	2d		,			VE		5162.338	I	2d?	20	?	1 4 4		IV	
5060.732	I	1 5		1			IV	112	5164.116	II	25	30				VE	1
5061.594 5063.435	II	3		6	1 2		VE		5165.073	I	1		1			IV	3
5065.537	I	$\begin{vmatrix} 3 \\ 2 \end{vmatrix}$		1			IV	37.5%	5165.338 5165.390	I	} 15		15?		1	IV	

 ${\it TABLE~A.} \quad {\it Temperature~classification~of~dysprosium~lines-Continued}$

Wave-	Spec-		1	Intensity			Temp.		Wave-	Spec-		I	ntensity			Temp.	
length	trum		C 1		Furnace		Class	Notes	length	trum	A	C l .	F	Turnace		Class	Notes
(Air)		Arc	Spärk	High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low		
5166.845	11	30					VE		5247.742	I	10d?					VE	
5168.110	I	2		2			IV	-	5248.141	II	20					VE	
5169.584	I	?		10			IV		5248.454	I	5					VE	
5169.688	II	150	60	10			VE	1	5250.804	I	2		2			IV	3
5170.193	II	5					VE		5254.158	11	1		1			IV	
5171.919	I	4		60			III	3	5255.047	11	15	20	_			VE	1
5172.895	11	5					VE	3	5255.326	I	1		1			IV	
5173.833	I	5		5			IV		5258.372	11	25	15				VE	1
5175.079	I	8d		6			IV		5259.880	I	30		20			III	
5177.575	I	1		1			IV		5260.558	I	100		80			III	
5180.105	I	3d		3			IV	7	5262.519	I	1		1		7	IV	
5182.231	I	1		1			IV	3	5263.546	I	?		2		7	IV	
5184.506	I	3		25			III	3	5264.354	I	6		5			IV	
5185.158	I	30		25			III	1	5265.746	I	2?		1			IV	
5185.615	I	1	,	1		1	IV		5267.111	I	80		100			II	
5186.984	II	2					VE		5268.949	I	3		5		-	IV	
5188.452	II	15	10	3			VE	1	5270.765	I	4	2.0	4			IV	1
5190.529	I	1-		4			IV	3	5272.248	H	80	30				VE	1
5192.496	I	?	400	2			IV		5274.068	I	20	100	60			II	,
5192.865	ΙΙ	1000	400	30			IVE	1	5275.291	II	100	100				VE	1
5194.053	I	1		3			IV	3	5275.916	I,	2					VE	
5196.814	I	6		$\begin{cases} 8 \\ 9 \end{cases}$			IV	2	5276.846	I	1 15		4			IV VE	
5196.969 5197.664	I	150	80	$\begin{vmatrix} & 1 & 2 \\ & 2 & 2 \end{vmatrix}$			IVE	3	5277.377 5277.684	II	4		6		,	IV	
5197.004	II	150	80	4			IVE	1	5277.883	I	8		6			IV	
5200.826	I	$\frac{1d}{2d}$		2			IV	7	5278.327	I	3		3			IV	
5200.820	I	$\frac{2a}{2}$					VE		5279.698	II	125	100)			VE	1
5202.334	II	1					VE		5280.391	I	2	100	2			IV	1
5205.663	I	10d?		10			IV		5281.594	I	1		1			IV	
5206.857	II	2		10			VE		5282.072	I	60		100			II	1
				(40			IV		5282.360	I	3		4			IV	
5212.033	I	3d		{ ?			?	14	5283.296	II	2					VE	41
5212.402	I	3		2			IV	13 -	5283.753	I	2		2			IV	100
5214.428	II	6d					VE	3	5284.987	II	50	30				VE	-1
5215.412	H	4			- 1		VE		5287.967	I	3		3			IV	
5216.212	I	1		6	-5		IV	3	5290.034	I	5		20		- 2	III	1
5216.427	I	1		4			IV	3	5292.713	I	2		2			IV	
5217.270	I	1		2			IV		5295.610	I	2		3			IV	3
5220.322	ΙΙ	(1?)				2	VE		5297.817	H	60	50	50			IIIE	1
5220.704	II	3					VE	, 1	5299.039	I	1		1			IV	١,
5221.980	I	10		60			IV		5300.298	II	20	8	50			VE	1
5224.228	I	1		5			IV		5300.884	I	5		50			III	
5225.028	I	1		1			IV		5301.576	Ι.	300		200			IV	
5225.867	I	1		1			IV		5303.170	I	3		1			IV	3
5226.919 5227.411	I	15		$\begin{array}{c c} 20 \\ 2 \end{array}$			IV		5305.727 5306.600	I	4		$\begin{array}{c c} & 1 \\ 2 & \end{array}$			IV	3
5227.411	I	$\begin{array}{c c} 1 \\ 3 \end{array}$		3			IV		5308.830	I	4		4			IV	
5227.827	I	$\begin{bmatrix} 3 \\ 2 \end{bmatrix}$		1	9		IV	3	5309.015	II	150	150	4			VE	1
5231.948	I	2d?		1			IV	,	5309.013	I	130	190	1			IV	3
5232.973	II	5		1			VE		5310.086	I	4		4			IV	
5234.275	I	1		1			IV	3	5311.849	I	3		15			IV	
5235.488	I	1		1			IV	3	5312.162	11	3		10			VE	
5236.253	I	25		150			I		5312.627	I	12		8			IV	
5238.372		5		50			III		5313.750	I	1		4			IV	1.50
	I		1				IV		5315.991)		5 0			VE	3
5240.894	I	2		1					5316.150	I			l i		į.	IV	
5241.463	· I	$2 \mid$		1			IV		5316.981	I	3		15	4		IV	1
5242.071	I			4			IV		5318.108	I	4		3			IV	
5242.485		3					VE		5319.202	I	4		6?			IV	3
5245.158	II	$2 \mid$					VE		5319.945	11	1					VE	3
5246.387	I	2	i const	3			IV		5320.619	I	1		1?			IV	
5246.944	II	20	20				VE	1	5321.689	I	8		6	10 10 10 11		IV	1.00

TABLE A. Temperature classification of dysprosium lines - Continued

Wave-	Spec-			Intensity			Temp.		Wave-	Spec-		I	ntensity			Temp.	
length (Air)	trum	Arc	Spark		Furnace		Class	Notes	length (Air)	trum	Arc	Spark	F	Turnace		Class	Notes
			- Cpuin	High	Medium	Low			(High	Medium	Low	-	_
5322.233	I	6		50			III		5425.304	I	2		1			IV	3
5324.695	II	125	125	2			VE	1	5426.336	II	2					VE	
5325.780	I	1		4			IV		5426.700	II	80	100	2			VE	1
5326.688		3					VE		5428.823	I	1		1			IV	3
5328.938	I	5		25			IV		5431.489	I	3		3			IV	3
5330.734	I	4	(10)				VE	1	5434.961	I	1		4			IV	
5333.083	I	5		5			IV		5436.678	II	4		1			IV	
5334.085	I	1		1			IV		5442.226	I	1		1			IV	3
5335.053	I	6		6			IV		5443.344	H	30	30				VE	1
5336.513	I	2		2			IV		5449.416	I	1		1			IV	3
5336.786	I	4		12			IV		5449.965	I	2		4			IV	
5337.432	H	30	20				VE	1	5451.109	I	300		200			I	
5340.300	I	100		80			III		5453.597	II	2					VE	
5343.154	I	4		20			IV		5454.249	I	2		3			IV	
5343.557	I	5		25			IV		5455.466	ΙΙ	40	40				VE	1
5345.562	I	2		1			IV		5455.711	I	3		10			IV	
5347.561		1					VE		5458.114	I	2		1			IV	
5348.353	H	4					VE		5459.340	I	2		1			IV	
5350.295		1					VE		5460.605	I	6		4			IV	
5352.114	I	40		150			II		5465.642	I	2		8			IV	
5353.245	I	3		3			IV		5468.641	I	1		1			IV	3
5354.993	I	3		?			IV		5469.106	ΙI	40	20				VE	1
5356.142	I	6		3			IV		5471.913	ΙI	15	(8)	20*) IVE	1
5360.665	II	2			× ×		VE		5471.961	I	13	(0)	20			(VI)	
5361.349	I	3		3			IV	3	5472.632	I	2		2			IV	
5364.852	I	2		1			IV		5474.888	I	2		2			IV	
5368.085	I	3?		2			IV		5477.253	I	4					VE	
5368.197	H	30					VE		5478.577	I	2		2			IV	
5369.245	II	5	(12)				VE	1	5479.925	I	3		2			IV	
5370.588	I	8		30			III		5481.112	I	1		2			IV	3
5372.980	I	4					VE		5481.637	I	2		?			IV?	
5376.099	I	10		6?			IV		5483.853	I	3		2			IV	1
5380.660	I	4		8			III		5486.382	I	3		2			IV	3
5381.358	I	2		25			III		5486.834	I	2		8			IV	3
5381.878		2					VE		5488.700	I	3		3			IV	3
5384.844	II	4					VE	3	5489.184		1					VE	3
5385.629	II	40	(14)				VE	1	5490.336	I	3		2		**	IV	1
5386.673		1		1			IV	3	5491.809	I	3		15			IV	
5389.580	H	300	(60)	3			VE	1	5496.181	I	1		1	7 5		IV	100
5389.744	I	?		15			IV		5496.830	I	20		20			IV	
5390.092	II	4			1		VE		5497.288	I	2		5			IV	3
5391.199	I	3		4			IV		5499.552	I	2		2	A		IV	
5392.044	I	15		50			II		5501.858	I	1		1		1. 1.	IV	1
5395.126	II	1		1			IV	3	5502.794	I	20		40		- 1	III	
5395.572	I	60		150			I		5503.927		2	1 1			-	VE	1000
5399.934	H	20	10				VE	1	5506.515	I	20		10			IV	
5401.354	I	6d?		4			IV		5508.301		5d?		2			IV	
5404.192	I	40		200			I		5511.313	I	4		3			IV	
5407.749	I	10		8			IV		5511.895	I	3		4			IV	
5409.681	I	3		3			IV		5515.407	ΙΙ	30	15	2		-	VE	1
5410.766	II	4d					VE	3	5519.925	I	5d?		2			IV	
5412.474		2		?			VE?		5521.762	I	2					VE?	3
5416.559	I	1		1			IV	3	5522.336	I	2		2	170	1	IV	3
5416.938	I	3		2		7	IV	111	5527.259	I	1					V	3
5418.722	I	4		3		121	IV	1 - 1	5527.443		3		00		100	VE	126
5419.133	I	80		60			III		5528.012	· I	30		80	100	7. 7.	III	197
5419.298	I	?		10			IV		5530.548	II	3		1			IV	1466
5420.770	I	8		60		12.44	III	37 70	5532.078	I	5d?		5		24	IV	
5421.989		2		3			IV		5534.367	I	4		4		12-156	IV	
5423.319	I	150		200			I		5535.216	I	8		5			IV	100
5424.273	I	20		20			III		5538.231	I	3		6			IV	
5424.699	I	2		1		1	IV		5539.100	I	1		2		1	IV	1

Table A. Temperature classification of dysprosium lines - Continued

Wave-	e		. 1	Intensity			Т		W/	e		I	ntensity			T	
length	Spec- trum		C 1		Furnace		Temp. Class	Notes	Wave- length	Spec- trum		6 1	1	Furnace		Temp. Class	Notes
(Air)	4	Arc	Spark	High	Medium ,	Low			(Air)		Arc	Spark	High	Medium	Low		
5542.195	I	8		. 4			IV		5656.327	ı	1		4			IV	3
5544.047	I	1		1?			IV		5658.785	I	2		4			IV	
5544.679	I	2		1			IV		5660.308	11	3	(5)				VE	1
5546.383	I	2		2		1	IV	3	5661.380	I	1		1			IV	
5547.268	I	300		300			I		5663.873	II	} 8d	(4)	5*			(VE	1
5552.861	I	2		2			IV	3	5663.954	I	$\}$ oa	(4)	3	100		liv	
5554.691		4		10			IV	. 3	5664.412	I	3		60		*	II	
5555.627	I	2	5	1		1.0	IV	1.5	5665.560	II	3					V	
5557.453	I	2		2			IV	3	5666.428	I	6		4	0.00		IV	
5559.119	11	8				2	VE		5669.268	, I .	- 1		- 1			IV	
5562.481	I	. 10		10			IV		5670.308	I	2		2			IV	
5563.169	II	8					VE		5671.250	I	20		20			IV	
5564.061	I	2		3			IV	3	5673.026	I I	2		4	-		IV	
5564.783	I	2					VE		5677.683	I	30		40			IV	
5566.302	I	5			1		VE		5678.344	II	6					VE	
5567.222		3	100	5			IV	×	5683.032	I	4		10			IV	
5568.150	I	5		4			IV	3 1 -	5685.583	I	40	-	300		5	II	
5573.943	I	1		1			IV	3	5687.625	I	2					IV	
5574.337	I	1		1			IV		5690.436	I	4		4			IV	
5575.951	I	2					V		5690.959	I	2		4			IV	3
5576.611	I I	2		40			III		5692.352	I	4		2			IV	1 -1
5577.817	I	1					V		5695.889	II	12	(8)	4			IVE	1
5579.432	I	1					V		5698.718	II	15	(15)		*		VE	1
5579.901	I	2		12			III		5699.332	I	20	,	200			II	
5582.799	II	1					V	3	5702.908	I	30	,	150			II	
5583.195	Į. I	8	(8)	30			III .	1	5704.458	I	1		2			IV	
5584.347	I	2		2			IV		5707.031	I	3		3			IV	3
5585.562	I	1	-	6			IV	1100	5707.808	I	20	1 3	25	11.0	. 7	IV	
5591.642	I	3		3			IV		5711.025	I	4		15			IV	100
5592.314	ΙI	5	(8)		,		VE	1	5713.848	I	2		5			IV	
5594.338	I	6,		4			IV	1	5717.686	I	3		4			IV	
5596.055	I	2					V	3	5714.925	I	2		2			IV	3
5597.350	ΙΙ	5	(5)				VE	1	5718.461	I	100		50		5.74	III	
5598.338	I	2?					V		5719.978	II	3		-			VE	
5598.799	I	1		3			IV		5727.451	I	8		50			III	
5600.652	II	200	(80)				VE	1	5732.912	I	15	*	12			IV	
5600.800	I	?		4			IV		5733.360	I	3		3			IV	
5602.426	ΙΙ	2					V		5737.704	I	3		3			IV	1
5605.629	I	20		20			III		5740.204	I	50		50			III	
5609.866	I	2		4			IV		5745.529	I	80		300			II	
5613.229	I	60		30			IV		5748.010	I	2		3			IV	
5618.453	II	1	1	0			V	3	5750.219	I	1?		6			IV	
5620.618	I	1		8			IV	2	5750.484	I	10		6		100	IV	
5622.498	I	3		4			IV		5753.648	I	5		2			IV	
5624.996	I	2		2			IV		5754.261	I	5		40	***		III	
5626.135	I	3		10			IV		5758.226	I	8		10	1.0		IV	
5627.490	I	20		200			II		5758.793	I	25		300			II	
5629.714	II	3					V		5759.780	I	4		2			IV	
5634.714	II	6					VE		5760.223	I	1		1			IV	
5635.976	II	2		4			V		5761.853	I	4	- 1	4			IV	
5637.160 5637.578	I	1		4			IV	2	5763.524	II	5					VE	
5639.498	I	500		400			V	3	5766.350	I	4		2			IV	3
5641.504	I	500	(10)	400			I	1	5766.973	II	5	100				VE	1
	II	25	(10)	2			IVE	1	5771.276	I	2		2			IV	3
5645.520	I	100		90		4	V		5784.026	I	4		6	4, , ,		IV	
5645.990	I	100	. 1	80			III	1 25	5787.197	I	5		5			IV	- 1
5649.766	II	3					V		5789.280	II	5					VE	0
5651.469	I	200		2			IV		5800.689		1		00			IV	3
5652.009	I	300	1.11	250	437		I	2	5802.617	I	8		80			III	
5653.488	I	2		2		1.2	IV	3	5805.554	I	30		100			III	
5654.543 5654.749	II	$\frac{1}{2}$		1	1 1		IV VE	$\begin{vmatrix} 3 \\ 3 \end{vmatrix}$	5807.658 5813.101	I	15 8		60			III VE?	

TABLE A. Temperature classification of dysprosium lines - Continued

			1	Intensity			_		NV.	C		I	ntensity				
Wave- length	Spec- trum				Furnace		Temp. Class	Notes	Wave- length	Spec- trum			I	Furnace		Temp. Class	Notes
(Air)	2	Arc	Spark	High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low		
5824.920	I	1		2			IV		5978.248	II	2	(2)				VE	1
5827.426	I	2		3			IV		5979.996	I	5	` ′	200			I	
5829.292	I	2		8			III		5982.501	I	3		5			III	
5831.378	I	1		1	4 y		IV	3	5984.102	I	1		3		,	IV	
5838.869	I	2		1			IV		5984.862	I	30		30			IV	
5840.125	I	5		8			IV		5985.990	I	15	,	100			II	
5840.339	I	5		1			IV		5988.562	I	800		500			I	
5845.360	11	8					VE		5989.671	ΙΙ	2				-	VE	
5846.157	I	4	, 1				VE		5990.505	I	1		3			IV	
5850.131	I	4	1	8	, to 1		IV		5991.674	I	8		50			III	
5852.460	I	4		6	100		IV	3	5992.638	II	2	<i>y</i>				VE	
5856.082	11	6	(6)				VE	1	5994.952	I	1		8	1 7 71		IV	
5856.976	I	2		10			III	3	5996.581	I	1		1			IV	
5858.054	I	2		3	1		IV		6000.838	I	10		10	1 × 1		IV	2
5859.566	II	4		20	1		VE		6001.214	II	1 15		20			VE	3
5864.025	I	15	2.5	20			IV	,	6003.262	I	15		30			III	9
5868.106	II	150	25	4			VE	1	6006.842	I	3		2	10.00		IV VE	3
5874.086	I	4		3			IV	3	6008.351	I	1 1		3			IV	
5876.312	I	1		4			IV		6008.938	I	40		250			II	
5883.216	I	2.		8			IV		6009.331	I	2		20			III	
5884.189	I	4		50			III		6010.815	I	200		400			I	
5887.497	II	4		20			VE		6013.638	II	3		400			VE	
5893.098	I	4		$\frac{30}{20}$	}		III	3	6017.263	I	20		150			II	
5893.308	I	6 5	,	20)		VE		6018.542	I	4		15	, .	1	III	
5897.670 5902.448	II	10	(10)				VE	1	6021.564	I	3		10			VE	
5902.446	II	5	(10)	6	27.7		IV	1	6023.593	I	1		4			IV	
5905.185	I	3		U	1		VE		6025.074	I	2		3			IV	
5907.262	I	$\begin{bmatrix} 3 \\ 2 \end{bmatrix}$		3			IV		6030.980	I	25		300			II	
5907.202	II	12	(7)	3	·		VE	1	6036.180	I	1		2			IV	
5915.163	II	100	(65)			10	VE	1	6038.700	ΙI	8					VE	
5916.619	I	5	(00)	5			IV	1	6040.443	I) ,		5			X	3
5922.360	I	6		6			IV		6040.556	I	} 1		15			III	3
5923.970	I	3					IV		6042.966	I	1		1		-	IV	3
5924.562	111	30	10	2			VE	1	6044.480	ΙI	4	(3)				VE	1
5927.812	I	5		3			IV	3	6047.051	I	1		2			IV	
5929.111	I	1		2			IV		6050.061	II	6	(4)		1.00		VE	1
5929.521	I) -					T.,,		6052.040	I	2		2		1, 7,	IV	
5929.591	I	} 5		6			IV		6052.914	II	4				27.0	VE	
5933.177	I	6		40			III	17 77 18	6053.201	I	1		5		17.76	IV	
5935.269	I	1		1			IV	13.1	6058.176	I	60		400			II	13. 13
5935.567	I	1		1			IV		6058.790	I	1	(0)	1			IV	
5936.597	I	3		3			IV	- 4	6063.561	II	8	(8)	150			VE	1
5938.816	II	2					VE		6073.775	I	10	(6)	150		- T Y _ F ?	II VE	1
5941.464	I	3		25			III			II		(6)					- 100
5943.674	I	8		150			II		6074.605	II	6	(4)			1.5	VE	1
5945.803	I	200	-41, -	300			II		6075.020	I	5		20		- 1 . v	IV	
5948.633	I	1		1			IV	3	6076.942	I	2		2			IV	3
5949.481	I	2	7 g - 7	2			IV		6079.843	I	1		1			IV	3
5951.614	I	2		2			IV	3	6083.362	I	2		4			IV	12.
5954.358	I	1		1			IV	3	6084.043	I	6		4			IV	
5955.514	II	5	(8)				VE	1	6084.372	I	1		2		-	IV	3
5958.803	I	1		1			IV		6085.056	I	100		500			II	
5961.272	I	5		5			IV		6088.261	I	500		400			I	
5964.464	I	100	15	400			II	,	6089.300	I	6		40			II	
5964.713	I	20?	15	40			III	1	6090.432	I	1		1			IV	
5965.052	I	1		12			IV		6090.889	I	10		200			II	
5965.426	I	1		2		4 72 1	IV	A Call	6091.270	I	2		200			VE	
5966.486	II	10		90			VE	100	6093.464	I	1		4			IV	3
5970.032	I	15		20			IV		6097.357		3		25			III	3
5970.719	II	300		300			VE		6099.646	I	6		80			II	

Table A. Temperature classification of dysprosium lines - Continued

W/	Spec-		1	Intensity			Т		Wave-	Spec-		I	ntensity			Temp.	
Wave- length	trum		C 1		Furnace		Temp. Class	Notes	length	trum		6 1	F	Turnace		Class	Notes
(Air)		Arc	Spark	High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low		
6103.375	I	10		125			II		6232.328	I	2					VE	3
6103.648	-	8					VE		6236.572	I	1					VE	
6106.201	I	1		3			IV		6237.391	II	2					VE	3
6107.621	I	10		15			IV		6238.268	I	3		6			II	3
6107.886	I	1		12			IV		6239.248	ΙI	8					VE	
6111.337	I	1		15			III	3	6240.171	ΙΙ	3					VE	
6113.927	I	15		50?			}II		6244.126	I	1					VE	
6114.074	I	10		200?			J	3	6246.847	I	40		8			III	
6115.276	I	15		150			II		6250.003	ΙΙ	5	(5)				VE	1
6115.676	I	10		80	2.		III		6250.654	I	10d		5			II	
6117.025	I	1		2			IV		6251.265	I	5		10			III	
6119.630	I	20		200			III		6254.309	I	6					VE	
6121.612	I	1		3			IV		6255.446	I	15		4			III	
6124.830	I	2		8			IV		6255.921	I	3					VE	
6125.931	I	1		4			IV		6259.088	I	1000		1200			I	
6126.487	I	30		40			IV		6260.364	I	}100		80			II	
6127.155	I	40		150			III		6260.444	I	J						1
6132.238	I	1		1			IV		6261.091	ΙΙ	2d		1			IV	
6133.645	I	60		300			III		6263.440	I	1		1			IV	
6138.362	I	8		40			III	3	6265.552	I	4		1?			IV?	
6142.211	I	1		10			III		6266.734	I	2		2			IV	3
6143.016	I	1		2			IV		6270.759	I	40					VE	
6144.879	I	2		1			IV		6271.102	I	20		3			III	
6145.537		2		2			IV	3	6272.897	I	5		2			IV	3
6146.441	I	1		2			IV		6273.800	I	15		4			IV	3
6150.604	I	10		40			III	3	6274.618	I	1		1			IV	
6150.772	I	8		80			III	,	6281.273	I	4		8			III	3
6151.488	I	3 1		$\frac{2}{2}$			IV		6283.738	ΙI	1					VE	
6152.770 6158.282	I	50d		400			II		6288.730	I	2		. 1			IV	3
6158.838	I	$\frac{50a}{1}$		5			IV		6290.485	II	5		40			VE	
6163.984	I	1		8	7		IV		6291.651	I	50		40			II	
6165.555	I	80		400			II		6298.902	I	3		_			VE	
6167.981	I	1		2			IV		6299.281	I	4		5			II	
6168.431	I	600		1000			I		6300.230	ΙΙ	6d					VE	3
6169.639	I	2		2			IV	3	6301.013	I	4		2			IV	
6170.317	I	3		3			IV)	6302.652	I	5					VE	2
6170.525	I	3		3			IV	3	6303.038	II	3		2			VE	3
6172.701	I	1		8			III	,			2 2					IV VE	
6173.454	I	2		6			IV		6305.150	I	1		20			III	
6175.173	I	2	7,7	2			IV		6305.626	I	2		1?			IV?	
6177.039	I	2	,	2			IV		6311.829	I	4		1:			VE VE	-
6184.704	11	4	(3)				VE	1	6316.632	II	5	(5)				VE	1
6189.706	I	10		100			III		6317.228	II	40	(20)				VE	1
6191.718	I	1	η.	?			VE?	3	6318.705	I	3	(20)				VE	1
6196.231	II	50	(25)				VE	1	6320.180	II	6					VE	3
6199.212	11	15					VE		6320.456	I	2					VE	
6203.382	I	2		1			IV		6321.464	I	5					VE	
6204.016	I	4		3			III		6322.793	I	3		1?			IV?	3
6205.120	I	1					V		6323.210	I	30		2?			IV?	
6206.322	I	2		1			IV		6326.912	I	6		5			III	3
6207.977	I	3		3			III		6329.216	I	8		6			III	
6210.767		2		3			IV						0				
6212.665	I	10		2			IV		6329.591	İ	3					VE	
6213.426	I	5		3			III		6331.086	I	30					VE	
6215.209	I	2	7 .				VE		6331.234	I	?		3			III	1
6216.562	H	6	(4)				VE	1	6331.988	I	4		2			IV	
6220.371	I	1		1	1		IV	3	6333.354	I	2d?	•				VE	10,2
6221.640	ΙI	2					VE		6333.814	I	4		4			IV	1
6225.371	I	3			į.		VE		6334.232	I	3		1			IV	
6229.740 6230.590	II	40		(2			VE		6336.121	I	1		•			V	
0400.090	I	} 10d		1 4			VE	3	6338.083	I	50		60			I	

TABLE A. Temperature classification of dysprosium lines - Continued

Wave-	Spec-			Intensity			Temp.		Wave-	Spec-		I	ntensity			Temp.	
length	trum		C		Furnace	12 5	Class	Notes	length	trum	Arc	Spark	F	`urnace		Class	Note
(Air)		Arc	Spark	High	Medium	Low	,		(Air)	-	Aic	эрагк	High	Medium	Low		
6339.318	II	5					VE		6444.149	I	10		2?			IV?	
6341.362	I	15		3			III		6445.489	I	1					V	
6341.877	I	3					V		6449.509	I	1					V	3
6342.518	II	6					VE		6449.974	I	10					V	3
6343.325	I	150		4			III		6450.501	I	20					V	
6344.689	I	3					V		6453.476	11	3					V	
6348.356	I	3		?			V		6454.587	I	1					V	
6349.002	I	2		1?			IV?		6454.886	11	1					V	
6351.251		3					VE		6456.019	I	3		2?			IV	3
6352.630	I	15		10			III		6459.260	I	3					V	
6353.090	I	15		2			IV		6460.048	I	1		1			IV	
6353.631	II	20	15				VE	1	6460.829	I	300		200			II	
6358.495	I	10		15	,		III		6467.943	I	2					V	3
6359.702	I	12		2			IV		6468.497	I	?		4			III	
6359.897	I	3					V		6468.576	11	150	(150)				VE	1
6361.496	ΙI	5					VE		6471.976	11	50	(35)				VE	1
6366.885	I	1					V		6474.005	I	1				7.	V	
6368.009		3				-	V	3	6474.915	I	125		1			VE	1
6369.590	I	80					VE		6478.218	11	15					V	
6371.997	I	1		1			IV		6480.961	11	4					V	
6373.157	I	2				-	V	3	6482.546	I	3		1?			IV?	
6374.439	I	3					V		6483.586	ΙI	300	(120)				VE	1
6375.010	I	12		12		1	II		6486.595	I	800		50			III	
6376.905		2				-	VE	3	6487.165	I	2					V	
6377.712	I	60					VE		6489.477	I	4		2?			IV?	
6379.323	I	5		2			IV		6496.265	I	1					V	3
6379.750	I	3		4			III		6498.528	I	2					V	
6381.368	I	5					V	3	6499.119	I	1					V	
6382.163		1					V		6503.472	I	1					V	
6386.796	I	400		300			I		6504.274	I	3		1			IV	3
6387.532	I	15		4			III	-	6505.318	I	5					V	3
6388.388	I	10		2			IV		6509.334	ΙΙ	3					V	3
6390.641	ΙΙ	10	(10)				VE	1	6511.474	I	1					V	
6396.411	I	?		?			II		6512.135	I	2					V	3
6396.604	11	200	200				VE	1	6513.126	I	15					V	
6402.009	I	10					V	3	6513.599	I	1					V	3
		50					V	0	6515.898	I	3					V	
6402.300	I								6516.527	ΙΙ	3					VE	3
6407.531	II	5					V		6517.909	I	1	(05.)				V	3
6408.274	I	3					V		6519.130	ΙΙ	50	(35)				VE	1
6410.397	I	2		-	/ /		V	1	6522.301	ΙΙ	4					V	
6413.500	I	6		1?			IV?		6526.026	I	4					V	1
6414.806	I	2	*	_			V		6527.963	I	3					V	3
6415.630	I	4		5			II		6529.453	ΙΙ	4	95				VE	1
6418.239	I	3?		1			IV }	3	6532.339	ΙI	10	25				VE	1,
6418.426	ΙΙ	30		= 00		91	VE S		6534.454	I	2	4 2				V	3
6421.917	I	600		500			I		6536.646	I	5					1 '	3
6423.070		2		100			V	0	6539.452	ΙΙ	8		15			VE	
6427.282	I	60		100			II	3	6542.608	I	10	(100)	15			II	1
6427.768	ΙΙ	6	(4)	_			VE	1	6548.258	II	200	(100)	4			VE	$\begin{vmatrix} 1\\3 \end{vmatrix}$
6431.180	I	3		2			IV		6550.750	I	5		4			IV	3
6432.399	I	1		1.0			V		6553.194	ΙΙ	8					V	
6432.965	I	20		10			III		6554.824	I	1					V	
6434.354	II	4					VE		6556.969	I	2		400			V	
6435.013	I	4					V?		6558.023	I	500		400			I	
6435.626	II	8	(8)				VE	1	6563.166	I	1					A	
6436.547	I	60					VE		6563.994	ΙΙ	5		7.0			V	1
6436.736	I	2?		2			IV		6565.114	I	150		10			IV	1
6441.815	II	6	(12)			100	VE	1	6570.196	I	3		2			IV	
6442.639	I	2				1 1 1	V		6574.299	ΙI	20			* . ¥*		V	
6443.085		1					V		6575.486	I	3			4.1		V	3

Table A. Temperature classification of dysprosium lines - Continued

Wave-	Spec-			Intensity			Temp.		Wave-	Spec-		I	ntensity			Temp.	
length	trum	Arc	Spark		Furnace	8.	Class	Notes	length (Air)	trum	Arc	Spark	I	Furnace		Class	Notes
(Air)		Arc	эрагк	High	Medium	Low			(AII)		Arc	Эрагк	High	Medium	Low		
6582.048	I	2	4			22	V		6709.519	I	1			^		V	
6582.979	I	3					V		6711.567	I	4		1			IV	
6583.523	I	1					V		6713.046	I	30		15			III	3
6585.079	11	2					V	3	6713.157	I		. *	13				
6587.503	I	5		5			IV		6716.200	I	2					V	
6591.678	I	15	(65)	2			IV VE	1	6718.266 6719.411	I	3		2			IV VE	3
6594.145 6595.299	II	80	(65)	1?			IV?	1	6720.216	I	1		1	1.0		IV	3
6595.581	1	1		1.			V .		6721.704	I	3		2			IV	3
6600.546	I	1					V		6722.238	I	1					V	3
6604.502	I	10					V		6723.210	I	1		2			IV	
6607.051	I	1		2			IV	3	6723.442	I	2		2			IV	
6611.729	II	15					V		6724.706	I	$\begin{vmatrix} 20 \\ 1 \end{vmatrix}$	-	5			III V	
6614.707 6614.911	I	$\frac{3}{20}$		2			V		6727.619	I	1	~		,		V	
6616.200	111	20					V		6730.337	1	1					v	*
6617.683	"	3				4	V		6733.823	I	3d?	* ,	2			III	3
6622.567	I	1	,				V	3	6736.069	I	15	,	20			III	*
6623.742	- I	1					V	3	6736.963	I	2	_	2			III	3
6625.490	I	15d?		6			IV		6738.569	I	3					VE	3
6626.972	I	2 3		2			IV		6739.860	I	3 2		4			III	
6628.288 6632.961	I	1		5			III		6740.470 6741.219	I	4		1			V	
6639.213	I	30		5			III		6742.274	I	5		5			III	D.
6641.450	I	2		2			III		6742.782	I	2		2			IV	1
6643.373	I	200	7.	250			I		6743.680	I	10					VE	3
6645.475	I	2		2			III		6744.439	I	8		2			IV	3
6649.522		2	×	2			IV		6747.930	I	300		100	х		II	
6650.290 6654.232	I	3 8	(8)	2			VE	1	6748.686 6750.212	I	$\frac{1}{30}$		40			V	
6654.542	I	1	(0)		1		V	1	6751.581	I	2		3			IV	
6658.039	I	10	2 -	40		-	III	3	6752.778	I	1			2 2 2		v	
6658.360	I	300		40			III		6753.052	I	1	*	1			IV	3
6660.090	I	1		3			III	3	6757.623	I	60		20			III	
6661.639	I	300		150			III		6758.489	I	1		1			IV	
6662.806	II	2					VE		6759.113	I	8 15		10 30	7		III	
6666.937	I	1200		4			III		6765.894	I	600		300			II	-
6667.858 6670.161	I	1200 30		800 40		-	II		6767.499	I	1		1			IV	
6672.061	I	1		1			IV		6768.037	I	2		2			IV	
6676.707	I	2	,	1			IV		6768.436	I	1		2			IV	
6682.094	I	3	A	2			IV		6769.790	I	2		1			IV	
6683.247	II	3					VE		6770.877	I	1	2	1			IV	1 3
6683.498	I	2		20	7 2 7		II		6772.188	I	5		6			III	
6684.776	ΙΙ	2		-			VE		6772.630 6774.088	I	1		2 3			III	3
6686.381	I	6		5			III		6774.590	I	4		5			III	3
6687.837	I	2 10		15	,	*	VE III		6775.078	ı	1		1			IV	
6688.068 6691.133	I	3		13 1			IV		6776.407	I	2		i			IV	
6692.351	I	2		1			V		6777.044	ı	15		30			II	
6692.729	I	4d?		2			IV	3	6777.646		6	,*				V	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
6694.072	I	2					V		6778.435	I	1					V	3
6694.568	I	3		2			IV	3	6780.997	I	1		1			IV	3
6697.028	II	1			e '1		V		6782.471	I	2		1			IV	
6698.122	I	1 4		2			IV	3	6783.082	I	3		1			IV	1 2
6698.401 6700.044	I	(1)		2	43		V	9	6783.942	I	$\frac{1}{3}$		1			IV V	3
6700.636	II	20	(15)				VE	1	6785.000 6785.701	I	4		15			V III	3 -
6701.582	II	1	(10)				VE	3	6787.370	I	25		20			III	
6704.333	I	2			* *		V		6790.298	I	30		200			I	
6704.724		1					V		6794.229	I	30	*	50			II	

TABLE A. Temperature classification of dysprosium lines - Continued

Wave-	Spec-		1	Intensity			Temp.		Wave-	Spec-		I	ntensity			Temp.	
length	trum		C 1		Furnace		Class	Notes	length	trum		6 1	F	Furnace		Class	Note
(Air)		Arc	Spark	High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low		
6795.167	I	1					V		6874.944	I	3		3			III	13
6795.538	I	2		1			IV		6875.122	I	10		2			III	}
6797.294	I	2					V		6875.823	I	2		2			IV	3
6797.552	I	5					VE?		6876.798		1		5			VE	
6798.937		2					V	3	6879.015	I	2		3			III	13
6799.579		2					V		6879.157	I	2		1			IV	}
6800.010	II	6					V		6882.313	I	3		1			IV	ľ
6800.419	Ι .	2		1			V		6884.315		1			,		V	
6803.066	II	8	(8)				VE	1	6885.939	I	1		1			IV	
6803.324	I	6		1			IV	3	6886.399	I	15		4	^ .		III	
6805.545	I	40		30			III	3	6888.565	I	6?		6?			IV?	3
6807.312		6	(5)				VE	1	6888.833	I	200		300			I	3
6808.409	I	2		. 1			IV		6889.859	I	1		1	7		IV	
6811.782	I	1	,	1	4		IV	3	6890.679	I	3		3			III	100
6814.839		4					VE		6891.205		1		,			VE	
6815.330	I	8		10	1.1		III		6894.516	I	25		10			III	. 0.5
6816.769	I	2			1 - 1		V	3	6895.228	I	1					V	3
6817.299	II	1					VE	3	6895.509	I	30		40			III	
6818.205	I	80		80			II		6895.953	I	2					V	
6818.680	H	2					VE		6896.905		1		1			IV	
6820.820	I	4	,	- 1	4	-	IV		6897.968	II	40	(25)	1			VE	1
6821.780	I	200		40			III		6898.923	I	20		8			III	3
6822.546	1	2				-	V		6899.321	ΙΙ	1500	1000	10			IVE	1
6822.687)							3	6900.040	I	1		6			III	
6824.703	I	1					V		6900.235	I	1					V	3
6826.438		1		1	X		III		6900.700	I	8	(4)	8			III	
6827.072	I	30		6			III		6902.046	II	4	(4)				VE	1
6828.347	II	6	(6)				VE	1	6904.076		1		1.5			V	
6829.130	I	2	,	1		,	IV	3	6905.949	I	3		15			III	
6832.914		1					V		6906.443	I	200	(110)	200*			(II	1
6833.652	I	8		8			III		6906.534	II	,					(VE	1
6835.418	I	2000		500	10		I		6908.419 6908.886		1. 1		,			V	3
6835.862	I	8?		8			IV		6910.386		3		$\frac{1}{2}$			IV	
6838.902	I	1			*		V		6912.198	II	10	(8)				VE	1
6839.563	I	3					VE		6912.677	II	2	(6)				VE	1
6841.191	I	1		1			IV		6914.002	II	2					VE	
6841.802	I	3					V		6915.340	I	2		1			IV	
6842.751		1		2			V		6915.784	II	1		1			IV	
6843.747	I	8 2		2	100		III		6917.213	II	î					V	
6844.970 6845.761		40		20	100		VE		6917.801	II	2					v	
6848.321	I	1	2	20			VE		6918.014	I	2		2			IV	
CO 40 FOO		2					V		6919.669	II	4					VE	
6849.593 6850.565	I	3	2		250	1	VE		6921.980	I	1		1			IV	
6850.803	I	1		1			IV		6922.845	I	1					IV	
6851.992	I	20		4			III		6923.204	II	1					VE	
6852.964	I	1500		400			II	5	6925.261	I	5		1			IV	3
6855.768	I	4		4			III	3	6925.494	I	10		3			III	3
6856.458	I	300		80			III	3	6927.664	I	1		1			IV	3
6857.356	I	1		00			V		6929.550	I	200		500			I	
6857.902	I	3		10			II		6931.517	I	1		1	1 2		IV	
6860.386	1	2		10		-	IV	3	6932.452	II	20	(16)	1			VE	1,3
6861.470	I	2		1			V		6933.865		1	(20)	1			IV	,,,,
6861.872	I	1				1	V	3	6935.778	I	5		2			III	
6863.394	I	1					VE	0	6936.963	1	1		1			IV	
6865.558	I	1					V.E.										1
6868.109	I	(?)					IV		6939.650	I	6	1.	3			III	
6870.893	I	8		3			IV	511	6940.242	I	2		4			III	3
6871.446	I	4	27. 21	1			V		6940.428	I	2			100		V	-
6871.819	1	2		1			V	3	6942.114	I	15		25	12.00		III	133
6873.020		1	300	1			VE	0	6945.263	I	20		150	1000	2102	II	
6873.636	I	2	275,34	3	1 2 2 3 3 5 5 7		IV		6946.432	I	3	P Y E	1	1 2 2 7 7 7	15/2/16	IV	

TABLE A. Temperature classification of dysprosium lines - Continued

TV.	6		1	Intensity			T		W	6		I	ntensity			Т	
Wave- length	Spec- trum				Furnace		Temp. Class	Notes	Wave- length	Spec- trum			F	Turnace		Temp. Class	Notes
(Air)		Arc	Spark	High	Medium .	Low			(Air)		Arc	Spark	High	Medium	Low		
6948.622	I	6		1			IV		7040.673	I	8		10			III	
6950.280	II	100	(80)	2			IVE	1	7043.622	I	10		15			III	
6951.417	I	50		8			III		7046.522		1					V	
6952.203 6952.933	I	3 10	(7)	1			IV VE	1,3	7047.485	II	3					VE	
6956.414	I	2	(')	2			IV	1,5	7049.446	I	3 3		2			III	
6957.483	I	10		6			III		7050.448	I	1		1			V	
6958.084 6959.687	I	1000		1000			I V		7053.577	I	6		1			IV	
6961.674	I	3		2			IV		7053.738	I	6		8			III	
6963.947	ΙI	1					V		7054.338	I	4		5			III	
6966.138	ΙΙ	1					VE		7054.644	I	3		,			V	
6966.984 6968.778	I	8 4		1 4			IV	3	7055.398		$\frac{1}{250}$	200	$\begin{vmatrix} 1 \\ 4 \end{vmatrix}$			IVE IVE	1
6970.427	I	80		100			II		7057.061	II	1	200	4			VE	1
6971.062	I	1		6			III	3	7059.680	ī	î					V	3
6972.871		1					V	3	7061.160	11	1		1			V	3
6973.594	I	10		2			IV		7061.814	I	2		2			III	
6974.677		1					V	3	7062.297	I	80		40			III	
6974.918	I	2		2			IV		7063.307	I	4		2			IV	
6975.436 6977.340	I	4 3		2			III		7063.887 7066.863	I	$\begin{vmatrix} 1\\2 \end{vmatrix}$		1?			IV?	
6977.932	II	6					VE VE	3	7067.840	I	$\frac{2}{2}$		1			VE	
6978.740	I	1					V	3	7073.036	I	4		4			III	
6982.435	I	150		60			III	1	7073.683	II	1		1?			IV?	
6984.364	I	2					VE		7074.683		1		1			IV	3
6985.506	I	2		2			IV		7075.139	ΙΙ	150	100	5			IVE	1
6986.191	I	3		3			III		7075.761	ΙΙ	2		١,			VE	
6990.077 6991.304		2 250		$\frac{1}{500}$			IV		7078.951 7079.661	I	$\begin{vmatrix} 1\\2 \end{vmatrix}$		$\frac{1}{2}$			IV	
6992.168	II	250		300			VE		7080.043	I	1					III V	
6993.160	I	6		2			III		7081.414	II	1					VE	
6994.914	I	3		1			IV		7082.090	II	1					V	
6996.450	11	1					VE		7084.228	1	1					VE	
6998.095	I	1500		800			II		7084.998	I	10		1			IV	3
6999.035	I	4		4			III		7086.245	I	2		1			IV	3
7002.732 7004.894	II	1 5		6			VE III		7087.590 7090.250		$\begin{vmatrix} 1\\2 \end{vmatrix}$					V VE	3
7004.054	II	2		0			VE		7091.733	I	5		2			IV	
7009.437	I	3		2			IV	3	7093.695	I	1	-	_	0		V.	
7012.303	11	3					VE		7095.649	I	2		5			III	
7014.640	II	8	(8)				VE	1	7095.858	I	4	1	2			III	
7015.608	I	2		1			IV		7097.791	I	3		3			III	
7017.416 7019.196	. I	400		200			II		7098.060	II	1?	4				VE V	2
7019.190	I	2		1		-	III		7098.800	II	3					VE VE	3
7020.907	I	2		2			IV		7099.725	I	1					V	
7021.783	I	5		10			III		7100.542	II	10	(10)			1.0	VE	1
7022.098	ΙΙ	1					VE?	1	7101.663	11	30	15				VE	1
7023.284	II	2					V		7103.516	I	3					VE?	
7026.032		2	,				V	-	7105.628	I	2					V	
7026.786	II	1		6			VE		7107.005	II	$\begin{vmatrix} 1\\2 \end{vmatrix}$		1			IV	
7027.283 7029.145	I	6 1		6			V		7107.357 7107.650	I	1		1			V	3
7029.143	1	$\frac{1}{2d}$					V		7107.050	II	100	60	15			IVE	1
7033.186	I	8		3	1 1		III		7110.079		1			1		VE	
7033.962	I	1		6			III		7110.987	I	2					V	3
7034.675	I	3		1?			IV		7111.611	I	2		1	1		IV	
7035.649	I	1		20			V		7113.054	I	3					V	
7036.375 7037.535	I	20		30			III		7114.710	II	1 5				1.	AL	3
7037.535	I	150 1		300			II		7116.289 7117.531	II	5					VE V	
7040.118	I	1		2			V	Sing !	7120.810	II	30					VE	13.73

 ${\it TABLE~A.} \quad {\it Temperature~classification~of~dysprosium~lines-Continued}$

>===				Intensity					di oj ayspr				ntensity				_
Wave-	Spec-				Furnace		Temp.	Notes	Wave-	Spec-				urnace		Temp. Class	Notes
length (Air)	trum	Arc	Spark		I		Class	Notes	length (Air)	trum	Arc	Spark			T.	Class	Notes
				High	Medium	Low							High	Medium	Low		
7121.232	I	150		500			I		7222.010	I	2		4			IV	
7121.895	II	130		300			VE		7222.520	I	10		1			IV	
7123.281		1					V	3	7222.901	I	15		100			II	
7125.363	I	2		1			III		7224.178		1					V	3
7126.251	I	1					V	3	7226.366	I	2		2			III	
7127.509	ΙI	1		_			V	3	7229.388	I	1		1			IV	3
7128.388	I	3		2			III		7230.044	I	600		400		-	II	9
7129.694	I	10		6			V		7231.591 7232.563	I	1 1					V	3
7131.368 7132.577	I	$\frac{1}{2}$		3			III		7233.270	I	1					V	
7133.381	I	6		4			III		7234.450	I	1		1			IV	
7135.430	•	2		•			VE	3	7234.679	11	8	. ?				VE	1
7135.896	I	3		1			IV	3	7237.664	II	1					V	3
×7137.521	I	4		4			III		7238.139	II	1					V	
7137.788	I	3		1			IV		7238.565	ΙΙ	1					V	3
7139.809	11	4d?					VE		7241.049	I	1			×		V	
7140.371		3					V	3	7243.051	II	2			7		VE	
7141.216	I	2	(0)	1	,		IV	,	7244.830	I	2					IV IV	
7141.515 7143.504	II	4 3	(3)	2			VE III	1	7245.870 7246.190		1 1					V	3
7145.066	I	4	(4)				VE	1	7247.001	I	1		1			IV	3
7147.251	I	1	(4)				VE	1	7250.010	I	300		400	1 1		Ī	
7149.302	II	6	(4)				VE	1	7253.398	II	1					VE	
7153.308		1	\ /				V		7254.601	I	3	-	2			III	
7155.838	I	2					V	2	7257.183	ΙI	1					V	
7156.478	I	40		15			III		7258.210	I	2		2			IV	
7157.300	I	1		1			IV		7258.562	I	4		2			IV	
>7158.742	I	3		3			III		7260.180	I	1		3			III	
7162.046	I	6		$\frac{10}{2}$			III		7261.738 7263.599	I	50 3		200			I VE	
7163.100 7166.502	I	1 15		20			III		7264.538	11	1			0		VE	3
7167.253	I	2		20	8		V		7265.576	I	1		1	8		IV	
7170.008	II	1					VE?		7265.889	II	2					VE	v
7170.478	I	3					V		7271.848	ΙΙ	2					VE	
7172.298	I	3		3			III		7273.573	11	20	(12)				VE	1
7172.690	ΙI	2	*				VE	3	7273.948	ΙΙ	2					VE	
7175.107	ΙI	60	(50)	1			VE	1	7274.249	I	2		5			III	
7177.791	I	2		1			IV		7275.508	I	1					V	
7181.372	I	2		3 3			(III)	3	7276.579	II	$\frac{1}{1}$					VE VE	
7184.102 7185.064	I	3		2			III	3	7278.597	I	1		1			IV	
7187.312	I	1		1			IV		7278.918	II	2					VE	
7190.080	I	2		1			IV		7279.710	I	2					VE	
7190.423	I	1		2			III		7279.905	I	8		20			III	
7192.657	I	20		5			III		7283.196	I	1		6			III	
7194.830	I	40		80			II?		7285.224	I	3	(7.0)	4			III	١.,
7196.709	ΙΙ	1		150			(V)		7288.238	II	20	(12)	60			VE II	1
7198.653	I	10		150			III		7288.921 7289.518	I	12 2		60			III	
7200.266 7204.248	I	1 1	10	,			V		7289.774	I	2		1			IV	
7206.279	1	1					VE	3	7291.048	I)						
7206.767	I	40		60			III		7291.140		3		2			III	
7207.328	I	40		100			II		7291.613	I	5		20			II	
7208.147	I	1		1			IV	3	7293.324	I	1					VE	
7213.274	I	150		200			II		7295.496	11	1					VE	
7213.899		1	A 2	1			IV		7297.897	ΙΙ	2					VE	2
7215.056	I	1		_			V		7298.662	I	2					VE	3
7215.513	I	15		5		1.1	III	3	7299.253 7300.276	II	$\frac{2}{30}$		40			VE	3
7215.940 7216.064	I	} 10d		$\begin{cases} 5 \\ - \end{cases}$			VE	0	7302.224	I	3	- 1	40	1/2 1		V	3
7217.744	I	4		15			III		7303.114	II	1					V	
7220.788	I	4d?		1	1		IV		7303.348	I	1					VE	

 ${\it Table A.} \quad \textit{Temperature classification of dysprosium lines} - {\it Continued}$

			* * 1	Intensity								I	ntensity				~
Wave- length	Spec- trum				Furnace		Temp. Class	Notes	Wave- length	Spec- trum			F	urnace		Temp. Class	Note
(Air)		Arc	Spark	High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low		
-						-							_				
7303.988 7308.976	II	1 1					V	3 3	7401.853	I	3		5			III (II	,
7311.425	I	1					VE	3	7403.103	II	100	(70)	150*			(VE)	1
7311.655	11	î					VE	3	7404.016	I	50		125			III	
7312.807	I	1					VE?	3	7407.595	I	150		500			I	
7313.079	I	1					V		7409.381	I	2		2			IV	
7313.405	I	2		1			IV	3	7409.708	I	2d		4			V	
7314.706	ΙΙ	2					VE		7412.369	I	400		300			II	
7318.170	H	1					V	3	7413.778	II	1					VE	
7318.704	H	2		9			V		7415.453	II	2		9			VE IV	8
7321.735 7322.269	I	$\frac{1}{2}$		2			IV .	3	7418.945 7422.561	I	2 2		2			IV	3
7324.195	I	3		1			IV	3	7425.219	I	3		1			IV	3
7326.843	II	1		1			VE		7426.194	I	3		2			IV	
7328.785	II	2					VE		7426.863	11	300	(120)	15			IIIE	1
7332.758	I	4		4			III		7427.553	11	1	()				VE	
7334.559	I	1					V	3	7427.889	I	20		40			III	
7336.886	I	2		2			IV		7428.538	I	30		8			III	
7337.454	I	1					V,		7429.370	I	3		2			IV	
7338.080	I	3		1			IV		7431.238	I	1					VE?	
7339.750	H	2					V		7433.140	I	6 <i>d</i>		2			IV	3
7340.081	I	4		4			III		7434.963	I	4d		3			IV	3
7341.077 7342.301	I	15 6		4			III		7436.568	II	3 4		4			V	
7345.132	I	150	(30)	20			III	1	7437.493	I	2		4			VE?	
7347.153	I	2	(30)	1			IV	1	7440.169	I	3					VE	
7349.147	I	1		î			IV		7449.502	ī	4					v	
7349.643	H	3					V		7450.489	I	6 <i>d</i>		1	,		IV	1 2
7350.475	I	2					VE		7451.115	11	30	(15)				VE	1
7351.031		1					VE	3	7451.802	I	3		2			III	
7353.582	I	20	80				II		7454.058	I	2					V	
7354.394	ΙΙ	6					VE	,	7454.760	I	4		_			V	
7355.574	II	1		4			V		7455.558	I	3	60	5	, ,		III	1
7357.065 7360.221	I I	$\begin{bmatrix} 5d \\ 4 \end{bmatrix}$	-	4			(IV)		7457.047 7457.864	II	100	60	3 2	* *		IVE IV	1
7361.578	II	8	(6)	1			VE		7457.804	I	60		50		-	III	
7362.779	II	6	(0)				VE	1	7461.759	I	3		25			III	
7363.590	I	1		1			IV		7462.158	1	1					V	1
7365.868	H	1					VE		7464.028	I	4					V	
7367.564	I	2		. 2			IV		7464.904	I	3					V	100
7368.566	I	2					V	3	7467.320	I	4		4			IV	
7369.045	I	15		60			II		7469.261		2			-		V	
7370.234	II	50	(35)	1			VE)1	7474.145	I	1		1			IV	L.
7370.447 7372.754	I	3 5		8 1			III	\frac{\int 3}{3}	7476.976 7483.027		1 100		20			V	
7376.038	I I	600	,	1000			I		7485.348	I	100		30 1			III	
7377.530	II	1		1000			VE		7487.479	II)		(-	-		VE	
7378.831	I	2	,	1			IV		7487.551	I	6		6			III	
7380.167		1					VE?	,	7490.790	I	10		2	- 2		IV	
7380.865	ΙI	2					VE	3	7493.771	I	12		10		7	III	
7381.566	I	150		300			II		7495.045	I	4		5			III	
7381.959	I	1					V		7496.184	I	3		7 - 6			V	
7386.184	ΙΙ	3	7	1			IV	*	7497.378	I	10		10			III	
7387.837	II	1					VE		7502.865	H	3					VE	
7388.166 7389.815	I	$\begin{bmatrix} 2 \\ 2 \end{bmatrix}$		1			IV V		7503.296	I	3					V	*
7391.172	II	$\begin{vmatrix} 2 \\ 2d \end{vmatrix}$					V	3	7503.872 7504.716	I	20 5		6			III V	
7391.547	I	$\begin{bmatrix} 2a \\ 2 \end{bmatrix}$, ,	1			IV	J		I						(VE	
7394.964	I	2	- 12				V		7506.475	II	8					(?)	
7398.276	I	(?)					III	3	7507.900		1					V	1
7400.660	I	3		30			III		7509.596	I	25		100			II	
7401.069	I	1		1			IV		7510.154	I	3		1			IA	

TABLE A. Temperature classification of dysprosium lines - Continued

			1	ntensity								Iı	ntensity				
Wave- length	Spec- trum				Furnace	-	Temp. Class	Notes	Wave- length	Spec- trum			I	Furnace		Temp. Class	Notes
(Air)	train	Arc	Spark	High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low		
					weatum	LOW	-				-			Wedium	Low	,	-
7512.580	I	1	(00.)	3			III	, ,	7626.587	I	4		1			IV	2
7516.613	II	15	(90)	3 5			IVE	1	7627.513	I	1 15		2 2			IV	3
>7519.469 7521.460	I	$\frac{4}{30}$		25			III	,	7629.575 7631.270	I	25		4			III	
7521.964	II	1.		20			VE	1	7633.618	II	23		-			VE	
7522.684	I	6		30			III		7635.320	I	40		4			III	
7523.863	11	4					VE		7638.171	I	2		5			III	
7528.506	11	3					VE	, 3	7639.298	I	30		15			III	
7529.595	I	3d	,	_			V		7640.004	I	4		1			IV	
7531.352	I	4		5			III		7641.093	I	800		600			II	
~7532.666	I	1004)	30 40			III		7641.226	I	3		4			III	3
7533.160 7533.698	I	$\begin{vmatrix} 100d \\ 3 \end{vmatrix}$		40			III		7644.273 7645.162	I	15		4 3			III	
7536.714	I	2			-		VE?		7645.866	I	150		150			II	
7538.921	I	4		1			IV		7646.637	ī	80	~	40			III	
7539.847	I	1		4	-		III	3	7647.153	I	1					V	
7540.340	- I	2					VE		7648.113	H	8	(7)				VE	1
7541.987	I	5		10			III		7650.435	II	1					VE	
7543.729	I	2000		1000			IV		7652.249	I	5					V VE	
7544.483 7544.992	I	2		$\frac{1}{2}$			III		7655.467 7661.478	II	?		200	,		I	
7545.916	I	3		2			V		7662.358	I	?		400			I	× .
7548.693	ī	3		3	-		III		7666.310	I	?		2			IV	
7553.000	I	300		100			III		7666.784	II	(15)?	(10)?				VE	1
7557.852	I	80	1,	150			II		7672.748	I	?		5			III	1.5
7559.036	I	1	5	2			III	3	7675.994	I	?		2			III	
7559.782	I	250	(160)	600			I	1	7676.687	I	40		40			III	
7562.965 7564.258	II	200	(160)	$\frac{4}{2}$			IVE	1	7677.481 7680.039	I	2?		2 2			IV	
7565.055	I	12d	,	3			III		7681.904	I	8		2			IV	
7566.979	ī	8		8			III		7682.715	I	8	*	8			III	
7571.370	11	2					VE		7688.665	I	?		2		1	IV	
7572.194	11	1		1			IV		7690.738	I	?		3			IV	1
7577.462	II	200	(120)	3			VE IV	1	7692.015	I	5?		5			III	
7578.454 > 7580.548	I	5 2		1 1			IV		7693.865 7696.540	I	8?		8 15			III	
7583.334	I	4		1?			IV		7699.838	I	?		3			III	
7584.748	II	1					V		7701.779	I	?		2	,,	,	III	
7585.364	II	3					VE		7706.666	I	?		3			III	
7587.764	I	25		15			III		7707.286	II	(2)?	(2)?				VE	1
7591.305	I	300	1 >	200			II		7710.137	I	?	12.	4			III	
7593.849	I	4	1 a	15			VE?		7711.912	II	8	(5)	200			VE	1
7594.859 >7595.408	I	60		15			IV		7715.327 7717.430	I	500		300			V	3
7596.280	I	5		5			III	,	7721.122	II	30d?		20			III	
7596.714	II	1					VE		7722.085	I	25		25			III	
7598.350	ΙI	2					VE		7724.378	I	2d					IV	
7598.686	II	1					VE		7725.582	I	. 3		3			III	
7603.724	· I	2d		1			IV		7728.020	I	5		_	*		V	
7606.506	I	5		1			IV		7728.758	I	4	(150.)	2			III	1
7609.175 7609.702	I	30		$\frac{6}{2}$			III		7729.764	II	200	(150)	. 8	1		IVE	1
7611.555	I	150		60			III		7732.516 7732.674	I	20d		15			III	
7612.725	I	150		4			III		7737.538	I	,		2	1 0		IV	
7613.433	II	1					V		7739.381	II	8	(5)				VE	71
7614.322	I	4		1			IV		7739.586	I	3		2			IV	}
7615.683	II	1	ř.	. 455			VE		7740.531	I	6		10			III	1
7616.215	I	50	· · · · · · · · · · · · · · · · · · ·	15			III		7741.916	I	2		1			V	
7617.702	I	100		15			V	1	7742.456	I	$\begin{vmatrix} 1 \\ 4 \end{vmatrix}$		1 4			IV	
7620.869 7624.290	I	$\begin{bmatrix} 2 \\ 4 \end{bmatrix}$			2.0	1,7 1, 1,	VE		7745.818 7746.671	I) 4		4			111	
7625.030	I	2	100	1			IV	4,5%	7746.836	I	} 2	De albi d	2	3763		IV	
	30177							1000			17			1	1		1

TABLE A. Temperature classification of dysprosium lines - Continued

W/	C		Intensity						Wave-	Snee		I		Temp.			
length t	Spec- trum	Arc	Spark	Furnace			Temp. Class	Notes	length	Spec- trum			Furnace				Note
(Air)				High	Medium	Low			(Air)		Arc	Spark	High	Medium	Low		
7750.148	,	50		150			II		7877.142	II	3					VE	3
7751.616	I	250	(125)	50			IIIE	1	7881.946	II	2		1			IV	
7753.115	I	1	(123)	30			A	1	7889.419	I	4		2			IV	1
7753.548	I	3		3			III		7893.992	I	2		_			V	3
7754.844	I	6		2			III		7899.750	I	5		40		-	II	
7757.324	I	40		150			II		7900.783	II	-d?					VE	
7760.083	I	12		6			III		7902.526	I	20		15			III	
7764.412	II	2		v			V	3	7904.520	ΙI	h		ſ -			VE	3
7767.119	II	2					VE		7904.629	I	3		1 2			IV	
7772.805		2					V	3	7908.860	I	?		4			III	3
7773.424		10		5			III	7	7909.386	I	300		150			II	
7775.783		5		40			II		7911.548	I	2		2			III	
7777.808	I	8		15			III		7916.739	I	30		200			I	
7780.890	I	100		40			III		7922.884	1	8d?					VE	
7785.811	II	2			1		V		7934.335	I	1		4			III	
7786.981	I	2		2			IV		7934.976	I	40		250			I	
7790.020	I	500		300			II		7940.672	ΙI	6	(5)				VE	1
7792.853	II	3					VE		7948.742	ΙI	5		-			VE	
7793.590	I	4		4			III		7952.244	ΙI	3		8	1		VE?	
7798.012	I	30		40			III		7954.178	I	8		8			III	
7799.247	I	2					V		7954.728	I	2		3			IV	
7801.618	I	4		4			III		7955.914	I	1		2			IV	
7806.967		1		8 (?)		III		7962.772	I	40		200			II	
7807.256	I	8			ĺ		VE		7965.413	ΙI	5					VE	
7808.114	I	3		4			III		7968.627	I	125		80			III	
7812.055	I	1000		300			II		7973.134	I	80		50			III	
7814.598	I	30		40			III		7982.854	-11	50	(40)				VE	1
7815.115	I	4		2			III		7983.415	I	3					V	<
7815.641	I	3		3			III		7990.087	ΙI	4					VE	
7817.765	11	1					V		7997.764	II	2					V	
7819.675	11	1					V		8004.474	ΙΙ	3					VE	
7821.103	I	4		1?			IV?		8008.706	ΙΙ	30	(20)				VE	1
7823.154	I	1					V		8010.194	I	40		50	/		III	3
7824.357	I	1					V		8016.845		4					VE	
7827.569	ΙΙ	3					VE		8025.312	I	80		400			I	
7828.052	I	2		1			IV		8027.216	I	50		20			III	
7829.060	ΙΙ	$\}$ 2d?					VE		8034.837	II	25	15	1			(V)E	1,3
7829.111	II)							8035.767	II	2					VE	
7830.893	I	1					V	3	8036.043	I	1		4	,		III	
7831.679	I	1		2			IV		8040.090	I	50		50			III	
7832.767	I	60		200			II		8042.664	I	2		30			II	
7833.877	I	20		40			III		8047.277	I	30		60			II	,
7835.522	ΙΙ	20	(15)				VE	1	8050.070	ΙΙ	10	(6)				VE	1
7836.012	I	1		1			IV		8050.853	I	30		40			II	1
7836.817	I	20		40			II		8057.988	I	4		1			IV	
7838.607	ΙΙ	3					VE		8059.959	II	2	1				VE	
7842.679	II	5					VE		8065.130	I	2		4			III	١,
7843.290	I	1		1			IV		8070.903	II	40	(20)				VE	1
7844.658	II	4					VE		8075.833	I	2		2			IV	3
7850.748	I	1		1			IV		8077.919	II	8	(8)				VE	1
7851.765	I	5		5	5		III		8098.335	II	8	(20)				VE	1
7858.624	I	2		2			IV		8106.308	I	15		25			III	
7860.768	I	8		6			III		8106.697	I	1		1			IV	,
7864.309	ΙI	30	(40)				VE	1	8108.430	II	50	(30)				VE	1
7864.965	I	100		80			III		8110.378	I	2		10			III	
7866.099	I	1		1			IV	3	8112.624	I	2		3			III	
7866.577	I	1		1			IV		8116.901	ΙΙ	30	(20)				VE	1
7867.617	II	3					VE	3	8121.354	ı, I	3		6			III	3
7870.638) I	10		2			IV		8123.707	I	6		3			III	<
7870.744	∫ I	8					VE(?)		8128.971	I	3		2			IV	1
7871.146	I	4		6			III		8139.706	I	5		4			III	
7874.934	I	3		2			IV	74.7	8140.724	II	4					VE	

Table A. Temperature classification of dysprosium lines - Continued

>=====	T						T							-		1	
Wave-	Spec-		, 1	Intensity			Temp.	Wave-	Spec-		I	ntensity			Temp.		
length (Air)	trum	Arc	Spark	Furnace			Class Notes	length (Air)	trum	Arc	Spark	Furnace			Class	Notes	
(2111)		Aire	Эрагк	High	Medium	Low			(1111)		1110	орили	High	Medium	Low		
8142.100	11	3					VE		8416.641	II	150					VE	
8144.295	II	6	(5)				VE	1	8424.557	ΙΙ	3 .					V	
8147.288	I	200	()	300			I		8435.476	ΙΙ	1					V	
8149.341	I	1		2			III	3	8438.583	ΙΙ	150					VE	9
8150.809	I	1		2			IV	3	8441.444	II	6					V VE	3
8153.797	I	3					V		8444.461 8448.860	II	60 5		5			III	3
8158.684	I	3		6 8			III	3	8455.503	II	5					V	
8160.317 8169.055	I	5 6d?		0			VE	3	8461.670	I	2		4			IV	
>8109.033 >8171.486	I	1		3			III		8462.225	11	1					V	3
8175.156	I	4?		3			III		8464.362	H	8d?					V	
8186.400	I			2			III		8472.580	II	40					VE V	3
8190.482	II	2?			1		VE?		8473.566 8477.784	I l I	2 4		15			III	
8197.290	I	2		2			III		8480.662	II	20		15			VE	.3
8198.770	ΙI	80	(25)	2			IVE	1	8490.149	ī	12		40			III	
8201.573	ΙI	300	(120)	30			IIIE	1	8492.370	11	10					VE	3
8204.928	11	1					(V)		8506.608	. 11	1					V	3
8208.339	H	8	(5)				VE	1	8507.817	ΙΙ	1					V	
8210.189	II	2					(V)		8510.792	II	150					VE VE?	3
8210.470	II	$\frac{2}{40}$					(V) VE	1	8513.273 8517.683	II	30 30					VE?	
8217.042 8218.623	II	125					VE	1	8521.105	I	3?		5			III	
8224.531	II	3					VE		8523.386	ī	1		20			III	
8225.130	I	5		150			I		8525.732	11	100					VE	
8233.557	II	40					VE	1	8527.295	I	1					V	
8235.379	ΙΙ	2					V		8528.326	ΙΙ	40		10			VE	9
8238.398	H	5d?		10			V		8537.398	I	1		10			III	3
8240.376 8240.948	I	$\begin{bmatrix} 1\\20 \end{bmatrix}$		40			III	-	8540.832 8540.958	II	3					V	3
8242.239	1	1		10			V		8548.931	II	50					VE	
8243.906	II	40d?					VE	1	8554.052	I	1		5			III	
8244.535	I	40		100			II		8557.786	11	50					(VE)	
8245.334	II	1		3			IV		8559.262	I	2		10			III	3
8246.867	I	10d		5 2			III		8563.430	I	2		20			III VE	3
8249.360 8255.076	I	6d?				1	V		8567.968	II	30 1?		2			III	3
8255.392	I	1					v		8573.013 8575.577	II	40					VE	"
8257.377	II	8					V		8578.664	I	5		6	, "		III	
8264.004	I	4		4			III		8582.638	I	5		40			III	
8265.528	I	200		600	^		I		8586.803	ΙI	8?			1		V	
8271.628	I	1		9			V		8593.202	ΙΙ	12					VE V	
8272.407 8284.146	I	$\frac{3}{3d}$		$\frac{2}{2}$			III		8605.201 8610.794	II	$\frac{1}{2}$		3			V	
8295.323	I	3		1			IV	3	8618.521	I	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		4			IV	
8302.283	I	2		5			IV	3	8622.556	II	6					V	3
8307.823	I	2?		2			IV	3	8625.315	I	2		3			IV	
8314.524				2			III		8630.118	I	25		80			III	3
8322.186	I	v		15 60			III	3	8632.429	ΙΙ	4					V	1
8323.849 8323.973	I	10		00			(V)	3	8635.778	II	60					VE V	3
8324.522	11	10					(V)	, "	8637.215 8655.935	I I	3 400					(V)	
8326.103	I	150		·1000			Ì	3	8657.678	II	200					(V)	
8335.313	ΙΙ	3					V	3	8667.375	II	50					(V)	
8341.519	II	2					V	3	8672.617	I	15		30			(III)	
8343.669	I	5		30			III	3	8678.490	ΙI	200					(V)	3
8344.351	II	4					V	3	8685.256	I	4		50			(III	
8346.571	I	3	* *.	1			IV	3	8696.829	II	50					(V)	3
> 8388.526	I	12		60		160	III		8715.949	II	25 1		5			(V)	
8392.008 8395.776	II	200	hiji ayara				VE		8728.538 8744.098	I I	2d?		10	- , .		(III)	
8395.776							VE		8750.400	II	50		10			(V)	3
0405.054	. 11	301							, 0.00.200								1

TABLE A. Temperature classification of dysprosium lines — Continued

Wave- length (Air)	Spec- trum	Intensity							Wave-	Spec-		Temp.					
		Arc	Spark	Furnace			Temp. Class	Notes	length	trum				Furnace		Class	Notes
				High	Medium	Low		11	(Air)		Arc	Spark	High	Medium	Low		
8753.513		3		2			(IV)	3	8912.567		8					(V)	
8759.043	H						(V)	3	8919.219		5					(V)	3
	II	6					(V)	3	8923.817		12					(V)	3
8762.120	I	2		3 2			IV		8924.814		10					(V)	3
8773.444	I	3		_					8924.814							1	
8780.831	I	25		60			(III)	3		H	15					(V)	3
8782.496	I	1		4			(III)	1	8970.763	I	8		3			(IV)	3
8783.524	I	3		4			(IV)	3	8972.248	11	10					(V)	3
8790.978	I	?		20			(III)	3	8985.667		5					(V)	3
8791.389	ΙΙ	100					(V)		8988.507	I	6		10			(III)	3
8798.378	I	2		3			(IV)		8994.150		2					(V)	- <
8805.409	I	10		15			(III)	3	9005.619		4					(V)	3
8809.869	I	1		3			(IV)	3	9014.103	ΙI	25					(V)	3
8813.492	I	3		4			(IV)		9020.789	11	200					(V)	3
8817.786	I	5		15			(III)	3	9038.596	I	25		50			(III)	3 -
8822.240	I	1		2			(IV)		9079.314	II	8					(V)	
8826.543		3	,				(V)	3	9100.495	I	3d					(V)	
8832.811	II	5					(V)	3	9111.168	11	200					(V)	
8833.083	ΙI	20					(V)	3	9136.428	11	4	-				(V)	_ <
8836.202	I	5		1?			(IV)	3	9169.436	ΙI	20					(V)	3
8836.863	I			2			(IV)		9171.587	11	600					(V)	
8842.633		4					(V)	3	9180.740	11	1					(V)	
8850.374	11	100					(V)	3	9182.318	I	15		10			(IV)	
8866.698	11	10					(V)	3	9200.275	11	15					(V)	3
8868.050	I	2		2			(IV)	3	9251.157	11	8					(v)	3
8873.610		4		_			(V)	3	9257.664	I	6					(V)	3
8897.212	I	10					(V)	3	9373.326	11	5					(v)	3
8905.748	II	80					(V)	3	9375.806	11	15					(V)	3
0,00,110	- 11	00					()		30.0.000		10					(•)	

Notes to Table A

Column 8

The Temperature Classification scheme used by King is as follows. (See Astrophys. J. 68, 200 (1928).

- The more decided low-temperature lines.
- II Lines that strengthen rapidly at medium temperature.
- Ш
- IV Lines requiring successively higher temperatures.
- A Denotes a neutral line that is relatively much stronger in the furnace than in the arc.
- E Denotes lines of ionized atoms (Dy II).

Column 9

- 1. See, also, A. S. King and C. E. Moore, Astrophys. J. 98, 33 to 42 (1943); "E" entered by present authors in Column 8 for lines from this reference, $\lambda 3002$ to $\lambda 8243$. This reference used for gap in 1956 list from $\lambda 3407$ to $\lambda 3463$ and $\lambda 3809$ to $\lambda 3831$.
- 2. See A. S. King, Astrophys. J. 72, 244 to 249 (1930); this reference used for gap in 1956 line list: λ3836 to λ3902.
- 3. Discordance in wavelength, LRL versus A.S.K. listing, exceeds ± 0.05 Å for wavelengths given to 2 decimal places by A. S. K.; ± 0.1 for those given to one decimal place.

References

- [1] A. S. King, Astrophys. J. 97, 323-380 (1943).
- H. N. Russell, J. Opt. Soc. Am. 40, 550-575 (1950).
- [3] F. S. Tomkins and M. Fred, Spectrochim. Acta 6, 139-143 (1954).
- [4] F. S. Tomkins and M. Fred, J. Opt. Soc. Am. 47, 1087-1091 (1957).
- [5] E. F. Worden, R. G. Gutmacher and J. G. Conway, Appl. Opt. 2, 707-713 (1963).
- [6] F. S. Tomkins and M. Fred, Appl. Opt. 2, 715-725 (1963).
- [7] A. S. King and C. E. Moore, Astrophys. J. **98**, 33-42 (1943).
 [8] A. S. King, Astrophys. J. **72**, 244 (1930).
 [9] A. S. King, Astrophys. J. **59**, 155-176 (1924).

(Paper 74A3-606)

Symposium on Electronic Density of States

Electronic Density of States was the subject of the 3d Materials Research Symposium, sponsored by, and held at the National Bureau of Standards, Gaithersburg, Md. on November 3–6, 1969. Attention was focussed on the correlation of various experimental and theoretical techniques such as optical methods; photoelectron, soft x-ray, and ion neutralization spectroscopy; specific heat; Knight shift; and magnetic susceptibility. Band theory and many-body effects, as they relate to the electronic density of states, were included.

Approximately 100 papers were presented at these sessions, including 16 invited presentations. Six of these invited papers were published in the March–April 1970 issue of the Journal, five are being published in this issue, and five will appear in the July–August issue. All of the papers presented at the symposium will be published by the National Bureau of Standards as Special Publication 323 which will appear later this year.